

Short Range Air Defense (SHORAD) **Engagement Performance Criteria**

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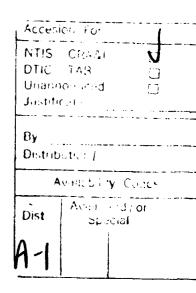
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| standards to develop to determ A review As a resu summary and displays, dures and difficulty this effo trainer. tests to difficult | This report presents and discusses the development, administration, and calibration of standards for qualification of Short Range Air Defense (SHORAD) operators. The objective is to develop range tables that the U.S. Army Air Defense Artillery School (USAADASCH) can use to determine the proficiency level of air defense soldiers for training and qualification. A review of the air defense literature and recent air defense empirical data was conducted. As a result of this review, air defense scenarios, scenario difficulty factors and weights, summary and task performance measures, performance scoring algorithms, performance feedback displays, air defense criteria cutoffs, and performance criteria test administration procedures and test conditions were developed. A preliminary examination of the scenarios, the difficulty indexes, and the criteria was conducted using field test data obtained during this effort using the Realistic Air Defense Engagement System (RADES), a SHORAD testbed and trainer. The preliminary performance standards will be subjected to a series of validation tests to ensure their representativeness and to further calibrate them according to scenario lifficulty level. | | | | | | | | |
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SHORT RANGE AIR DEFENSE (SHORAD) ENGAGEMENT PERFORMANCE CRITERIA

EXECUTIVE SUMMARY

Requirement:

To determine operator engagement task and summary performance parameters, scenarios, scenario difficulty scaling factors, performance measures, performance scoring, and performance criteria, and test administrative procedures for applying qualification standards to Military Occupational Specialty (MOS) 16P, 16S, and 16R soldiers. The required research products combine to form the Short Range Air Defense (SHORAD) systems performance criteria and applications procedures.

Procedure:

The draft SHORAD performance criteria were determined by means of the analysis of field test and experimental data collected in the Realistic Air Defense Engagement System (RADES) testbed and trainer. A scenario difficulty weighting procedure was employed to assess agreement between empirically defined scenario difficulty indexes and scenario difficulty ratings ascribed by subject matter experts.

Findings:

Results obtained from field test experiments and the RADES multi-experiment database were used to determine engagement performance standards attainable by SHORAD personnel. Performance variations were consistent with expert ratings in determining scenario difficulty levels. Multidimensional performance criteria and scenario difficulty scales were determined and will be subjected to empirical validation.

A fully integrated and automated, scenario-specific feedback and multiscenario scoring system was also developed and tested. Over 200 training and test scenarios were developed and indexed by performance difficulty level. Performance criteria cutoffs and administrative procedures have been outlined, implemented, and tested, in anticipation of future validity testing.

Utilization of Findings:

The proponent for this research was the Directorate of Training and Doctrine (DOTD), United States Army Defense

Artillery School (USAADASCH). These results and draft standards were briefed to the Director, DOTD, on 26 September 1988. This research will form the basis for draft standards of performance for SHORAD crews in associated gunnery tables.

SHORT RANGE AIR DEFENSE (SHORAD) ENGAGEMENT PERFORMANCE CRITERIA

CONTENTS

| | | | | | | | | | | | | | | | | | | | | | | | | | Page |
|------------------|-------|------------|------|-------|------|----|------------|------------|-------|-------|-----|-------------|------------|------|-----|-------|-----|-----|-----|----|---|---|---|---|-----------|
| OVERVIEW | | | • | • | • | | • | • | • | • | • | • | • | | | | • | • | • | • | • | • | • | • | 1 |
| Operat | iona | 1 F | Prob | ole | m | | _ | _ | | | | | | | _ | | | | | | | | | | 1 |
| Resear | cch C | bie | ect | ive | 2 | • | • | • | • | • | • | | | • | • | | | • | • | | • | • | • | | ī |
| | | | | | | | | | | | | | | | | | | | | | | | | | 2 |
| Approa RADES | • • | | • | • | • | • | • | • | • | • | • | • | • | • | • | • | • | • | • | • | • | • | • | • | 2 |
| BACKGROUN | 1D . | | • | • | • | | • | | • | • | | • | • | | • | | • | • | • | • | • | • | • | • | 5 |
| FINDINGS | AND | PEF | RFOI | RMA | NC | E | CF | RI: | rei | RIA | A (| 201 | 4PC | INC | ENT | rs | | | | | • | • | • | • | 7 |
| Multi- | -Expe | erin | nent | t D | at | ab | as | se | Ma | ana | aae | eme | ∍nt | c a | and | 1 2 | ۱na | alv | vs: | is | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | 7 |
| Res Defini | itior | n of | s s | cen | ar | ic | [`כ | e: | st | Co | ond | lit | tic | ons | 5 | • | • | • | | | | | | | 22 |
| Scenar | cio s | Scri | bt: | ina | r a | nd | l | ei | 1ei | rat | ic | on | | | | | | | | | | | | | 22 |
| Scena: Summa: | y ar | nd I | ras) | κP | er | fc | rn | nai | 106 | e 1 | 1ea | as | ıre | es | De | ef: | in | it: | ioi | ว | | | | | 24 |
| Scori | ng Al | lgor | rith | am. | De | ve | 210 | ıgo | nei | nt | | | | | | | | | | | | | | | 27 |
| Scenar | cio E | eed: | dbad | ck | Di | sp | 1 a | ī | De | efi | ini | it: | ior | 1 | | | | | | | | | | | 30 |
| Deterr | ninat | cior | 1 0 | £ S | ce | na | ıri | ĺŌ | D: | iff | fic | cu] | Lty | 7] | Fac | cto | ors | 3 | | | | • | • | • | 36 |
| Scenai | cio E | Fiel | ld : | res | ti | no | ſ | | • | | | | • | • | | • | | | | | | | | | 37 |
| Scena: Deterr | ninat | cior | 1 0 | f S | PM | a | inc | 1 : | ΓPI | 4 (| Cut | :- 0 | ofi | E S | Sco | ore | es | • | • | • | • | • | • | • | 47 |
| REFERENCE | ES . | | | • | • | • | • | • | • | • | • | • | • | • | • | • | • | • | • | • | • | • | • | • | 51 |
| APPENDIX | λ | סייים | S | ואיםר | ם גז | т^ | . т | т, | י כוכ | N D N | , , | . | . . | דגיו | 201 | em. | | | | | | | | | |
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| | | | | | | | Ъ | TS | T | OF | T | AB | نظيا | S | | | | | | | | | | | |
| Table 1. | Dep | end | lent | t v | ar | ia | bl | .es | 3 | • | • | • | • | • | • | • | • | • | • | • | • | • | • | • | 10 |
| 2. | SHC | RAI |) sı | ımm | ar | У | рe | ri | 01 | cma | nc | e | da | ata | à | • | • | • | • | • | • | • | • | • | 12 |
| 3. | | eve ent | | ra | ng | es | а | nc | l p | er | fc | rn | nar | nce | e c | ut | cc | ome | es | by | 7 | | | | 12 |

CONTENTS (Continued)

| | | Page |
|-----|--|------|
| 4. | FW event ranges (in kilometers) and performance outcomes by model type | . 13 |
| 5. | RW event times (in seconds) and performance outcomes by intent | . 14 |
| 6. | RW event times (in seconds) and performance outcomes by model type | . 15 |
| 7. | Fixed-wing event range comparisons (in kilometers)Wright (1966) versus RADES (1987) . | . 20 |
| 8. | Fixed-wing event range comparisons (in kilometers) for the A7 and A10Tillapaugh & Smith (1983) versus RADES (1987) | . 20 |
| 9. | Friendly rotary-wing event time comparisons (in seconds)Lott (1977) versus RADES (1987) . | . 20 |
| 10. | Helicopter event time comparisons (in seconds) for the AH1CDEC (1978) versus RADES (1987) | . 21 |
| 11. | Recommended test conditions | . 23 |
| 12. | Recommended aircraft | . 24 |
| 13. | Candidate summary performance measures (SPM) | . 28 |
| 14. | Candidate task performance measures (TPM) | . 29 |
| 15. | Scoring transformation algorithms for RW time data | . 32 |
| 16. | Scoring algorithm output | . 33 |
| 17. | Standardized scenario set | . 38 |
| 18. | Scenario presentation sequence | . 38 |
| 19. | Dependent variables | . 39 |
| 20. | Summary performance results by target type and intent | . 42 |
| 21. | Summary performance results by each subsequent RW target worked | . 43 |

CONTENTS (Continued)

| | | Page |
|-----------|--|------|
| Table 22. | Effects of RW scenario variations on performance (significant Pearson correlations) | . 44 |
| 23. | REsults of \underline{t} test comparisons of performance by difficulty level (two-tailed test using separate sample variances) | . 45 |
| 24. | Relationship between difficulty level and performance (significant Kendall and Spearman correlations) | . 45 |
| 25. | SPM cutoff values estimated from RADES research results | . 48 |
| 26. | TPM cutoff values estimated from RADES research results | . 49 |
| C1. | Scenario descriptive statistics | . C1 |
| | LIST OF FIGURES | |
| Figure 1. | FW engagement event sequence | . 16 |
| 2. | RW engagement event sequence | . 16 |
| 3. | Distributions for FW events (kilometers) | . 17 |
| 4. | Distributions for RW events (seconds) | . 18 |
| 5. | Range layout | . 25 |
| 6. | Fixed-wing scenario feedback screen | . 34 |
| 7. | Rotary-wing scenario feedback screen | . 35 |

SHORT RANGE AIR DEFENSE (SHORAD) ENGAGEMENT PERFORMANCE CRITERIA

OVERVIEW

Operational Problem

At the request of the Directorate of Training and Doctrine (DOTD) of the US Army Air Defense Artillery School (USAADASCH), and with the suport of the US Army Missile Command - Target Management Office (MICOM-TMO), the Army Research Institute is developing a Range Target System (RTS). The RTS provides sustainment training, qualification, and certification of Short Range Air Defense (SHORAD) crews, teams, and operators in engagement simulation and live fire exercises. The RTS will also support future Forward Area Air Defense System (FAADS) components. These include the Line-of-Sight-Foward-Heavy (LOS-F-H), Line-of-Sight-Rear (LOS-R), and Non-Line-of-Sight (NLOS) weapons system and the Forward Area Air Defense Command, Control, Communication, and Intelligence (FAAD C³I) system.

A critical component of the RTS will be the range tables, the basis of which will be derived under this program of research. The RTS configuration and this research effort are interdependent projects. The RTS promises to be the means of institutionalizing range table procedures, scenarios, performance measures, scoring, and performance criteria in a way that will improve ADA collective crew readiness Armywide. The range tables and associated RTS are expected to be fielded as an integrated product to ensure an objective crew sustainment and qualification program of training and evaluation.

The product of this research will be valid, reliable, practical, and economical engagement performance range tables for use in SHORAD crew, team, and operator sustainment training and qualification testing, which are compatible with the emerging Range Target System.

Research_Objective

The research objective is to determine the range table components. First, test and training scenarios are needed. Second, performance difficulty level indexes are needed to partition the scenarios for training and test purposes. Third, engagement performance task and summary performance measures are required to diagnose the errors. Fourth, engagement performance criteria (i.e., performance standards) are needed to quality soldiers and to establish minimum acceptable levels of performance. Fifth, range table administrative procedures and scenario feedback, across-scenario scoring algorithms, displays, and hardcopy report formats are needed to ensure proper utilization and information payoffs from the application of the range tables.

Approach

The approach was to repeat a pre-defined sequence of subtasks until the research objective had been successfully attained. These subtasks were:

- Scenario Scripting and Generation
- Scenario Administration Conditions Specification
- Summary and Task Performance Measures Specification
- Scoring Algorithm Development
- Scenario Feedback Display Definition
- Hardcopy Multi-Scenario Scoring Report Development
- Expert Rating of Scenario Difficulty Factors
- Collection of Individual Soldier Differences Data
- Field Test Data Collection
- Multi-Experiment Database Management and Analysis
- Target Parameters and Distribution Specification
- Field Test Data Analysis

Soldiers served on an as available basis. Subtasks were performed in various sequences to capture meaningful soldier performance data. Fortunately, the Realistic Air Defense Engagement System (RADES) already had the task and summary performance measurement capabilities needed, so field test performance data could be captured and stored for later use in range table development and verification. The RADES testbed was therefore employed to meet essential data requirements.

RADES

RADES is an instrumented testbed and SHORAD engagement simulation exercise (ESX) system. SHORAD soldiers employing their actual weapon systems engage scaled fixed wing (FW) and pop-up rotary wing (RW) aircraft in an outdoor desert environment under controlled field test conditions. As many as five weapons and their associated crews, teams, or operators can be tested or trained at a time. Direct weapon connections automatically collect interrogation friend or foe, acquisition, track, lock-on, uncage, superelevate, fire, and launch signals from the weapon. Detection, identification, and command to engage or cease engagement voice commands are collected using human data collectors at computerized data acquisition stations. The human data collectors enter event data via the data collection station keyboard.

ADES synthetically flies missile rounds to target intercept and evaluates the outcome as a kill or miss, predicated on the status, location, and range of the aircraft at time of intercept. Time delays in software ensure that effects are not provided to the weapon team or crew until the intercept would have occurred under fullscale conditions. RADES automatically records the reason for any assessed engagement miss (e.g., aircraft out of range, failure to acquire, no lock-on at fire, failure to superelevate, etc.). The RADES host computer provides aircraft status, location, and range data to the data collection stations during realtime engagements. The host also collects and consolidates the data into an aggregate test file at the end of every engagement trial. It is this aggregate data file that is returned from the field site for database management and analysis.

RADES research has demonstrated the following situational effects on air defense performance (Barber, 1987):

- Target Characteristics
 Aspect, elevation, azimuth (offset), size, type, and range
- Weather and Terrain Conditions
 Visibility, weapon position, target background (contrast), atmospheric conditions (wind, temperature)
- Individual Differences
 Sensory, perceptual, psychomotor, cognitive, and personality
- Level of Training and Scenario Difficulty
 Experience, workload, and practice level
- Command, Control, Communications, and Intelligence (C3I) Alerting, cuing, reliability of information
- Doctrine and Tactics

BACKGROUND

In many ways this research is directed at correcting current deficiencies in existing engagement performance criteria, criterion-referenced standards, qualification scenarios, and test administration procedures. Current engagement qualification and training criteria and standards of engagement performance are deficient in the following ways:

- Counterair Effectiveness (ordnance delivery prevention is not considered by existing scoring procedures).
- Friendly Air (the effects on performance of complicating friendly air elements and corresponding fratricide rates are not included in current qualification and certification testing processes and standards for all SHORAD systems).
- Task Difficulty (the significant effects of scenario- and environment-imposed task performance difficulty are not considered in the development and ordering of scenarios for test and training purposes).
- Achievable Performance Levels (criteria have not been developed, nor are they administered, with consideration of achievable soldier performance levels).
- Collective Crew Engagement Performance testing and qualification (current standards are directed solely at gunner part-task qualification and do not include crew chief, squad leader, or team chief tasks).
- Test Administration Controls and Procedures, qualification test scenarios, and test conditions (current qualification and certification testing procedures are subject to a large amount of user interpretation and vary considerably in test administration practices and environmental conditions from one application and unit location to another).

To overcome these weaknesses in current engagement performance qualification and certification testing, ARI, at the request of the Directorate of Training and Doctrine (DOTP), formulated a comprehensive approach to formal range table development.

As a result, the present research has given rigorous attention to those factors not normally addressed, or only modestly treated, in the determination of previous qualification standards of performance. These contributions include the:

- Crew, team, and operator distribution parameters for each Summary Performance Measure
- Impact of using a weapon control status of "tight" versus "free"
- Effect of introducing multiple targets simultaneously or sequentially
- Effect on Summary Performance Measure scores of introducing friendly aircraft
- Effects of including the squad leader
- Impact on crew performance of including an ordnance delivery prevention criterion
- Effects of various types of alerting and cuing
- Consideration of soldier capability limitations which affect performance

FINDINGS AND PERFORMANCE CRITERIA COMPONENTS

This section describes the requirements, procedures, and findings for all the subtask actions conducted in this study. Specifically addressed are the:

- Multi-Experiment Database Analysis
- Definition of Range Table Scenario Test Conditions
- Range Table Scenario Scripting and Scenario Generation
- Definition of Summary Performance Measures (SPM) and Task Performance Measures (TPM)
- Scoring Algorithm Development
- Scenario Feedback Display Definition
- Determination of Scenario Difficulty Factors
- Scenario Field Testing
- Determination of SPM and TPM Cut-off Scores

The report includes a discussion of findings directly addressing the future actions toward fielding of the SHORAD sustainment training and qualification testing range tables.

Multi-Experiment Database Management and Analysis Results

Requirement: To establish baseline performance parameters for Short Range Air Defense (SHORAD) system crews, teams, and operators, and to generate databases on human performance from which to draw generalizations about the ADA population.

Procedures: Air defense engagement part-task and summary performance efficiency and effectiveness were measured under a wide variety of environmental and scenario test conditions using the RADES testbed over a period of two years. Individual difference measures on participating soldiers were also obtained coincident with those experiments contributing to the RADES multi-experiment database.

Test Conditions: Analyses were based on prior test results obtained from RADES experiments. The experimental conditions existing during these tests were clear weather, daylight conditions. Data reflected the performance of SHORAD crews and teams reacting to 1/7th scale, flying fixed wing (FW) aircraft and 1/5th scale, pop-up rotary wing (RW) aircraft. Results from the following field tests were consolidated to produce a meta-analysis.

- Chaparral Weapon Control Status and Identification Friend or Foe (IFF) Experiment
- Redeye Weapon Control Status and Training Experiment
- Stinger Terrain and Target Characteristics Experiment
- Stinger Early Warning and Cuing Experiment
- Tripod Mounted versus Man-Portable Stinger Experiment
- Enhanced RADES Observer Experiment
- Stinger Training Experiment

Table 1 presents the dependent variables used in the metaanalysis. Average scores for these variables were derived based on weighted means with extreme outliers (i.e., + or - 3 standard deviations) removed. Average scores were derived by taking the mean of all observations for a single crew or team for a given scenario type. Therefore, while multiple observations were obtained from each crew, the sample sizes reflect the total number of crews participating, not the total number of observations.

These past investigations focused upon different experimental manipulations and controls. Hence, the results presented in this section should be viewed as the overall, expected performance of the SHORAD population aggregated across weapon systems and experimental conditions. These conditions included:

- Weapon systems (Stinger, Chaparral, and Redeye)
- Experience and training level (trainees to NCOs)
- Target aspects and offsets (face, tail, and side views)

- Target approach azimuth and flight profile
- Target background (sky versus terrain)
- Early warning and cuing (varied in method, delay time, update rate, content, and accuracy)
- Alert status and weapons control status ("red free", or "red tight")
- Rotary wing range (2.5 km to 7 km, fullscale)
- Soldier differences (vision, demographics, and personality)

Table l Dependent Variables

| CODE | TITLE or DESCRIPTION | DUTY | INTERPRETATION |
|-------|---|-------------|---|
| RDET | Range of Detection | SL or SG | The slant range from the weapon to the target when the event |
| RID | Range of Identification | SL | took place. Range is relevant for fixed wing targets only |
| RLOCK | Range of Track or Lock-on | SG | since rotary wing targets simply popped-up from a static position. Panges |
| RFIRE | Range of Weapon Fire | SG | are given in full scale kilometers. |
| TDET | Time of Detection | SL or SG | Based on seconds after target availability where availability begins when visual line-of-sight is achieved. |
| TID | Time of Identification | SL | Time interval between Detect and Identification |
| TLOCK | Time of Lock-on | SG | Time interval between Detection and Lock-on. |
| TFIRE | Time of Weapon Fire | SG | Time interval between Lock-on and Fire. |
| THAND | Time of Handoff | Both | Time interval between Identification and Fire. |
| TTOT | Total Engagement Time | Both | Time interval between Detection and Fire. |
| IDCOR | Correctness of Identification | SL | Number of correct identifications divided by number of targets identified. |
| PKILL | Probability of Target being engaged and destroyed | Both | Number of aircraft destroyed divided by number presented. |

KEY: SL = Team or Squad Leader

SG = Senior Gunner

Findings: Data from the first set of single target (FW and RW) trials from several RADES tests were consolidated. From these consolidated data, engagement parameters were estimated. The performance data provided herein represent overall results drawn from two years (1985 and 1986) of RADES experiments.

Table 2 lists summary performance results for the SHORAD population for FW and RW targets in terms of overall engagement outcomes. Table 3 provides FW aircraft ranges in full scale kilometers for critical engagement outcomes as a function of aircraft intent (hostile or friendly). Table 4 provides these data relative to aircraft intent for each model type. Table 5 presents the approximate RW aircraft event times in seconds for critical engagement outcomes as a function of aircraft intent. Table 6 presents these data as a function of aircraft intent for each model type. Blank spaces in these tables indicate that the data were missing or the sample sizes were too small to be meaningful.

All rotary wing event times were based on the time when line-of-sight (LOS) was first established. LOS was defined as the point in time at which the helicopter rotor blades first broke the terrain masking. The entire helicopter became visible approximately 2 seconds after that.

Engagement Parameter Estimates: The fixed wing engagement event sequence and the rotary wing engagement event sequence have been depicted in Figures 1 and 2, respectively. These figures show approximate population parameter values associated with critical engagement part-task events by target type (FW or RW), and illustrate how these events unfold. The greatest potential for improvement in engagement performance can be afforded by increasing the range at which aircraft are detected, identified, and acquired. Smooth tracking, lock, and fire task actions are rather tightly grouped in terms of their time and range of occurrence. Thus, if the range of detection, identification, and acquisition are extended, the subsequent ranges of track, lock, and fire will result in greater ranges of engagement.

Figures 3 and 4 depict the overall expected distributions of the SHORAD population with respect to FW and RW engagement events, respectively (assuming a normal distribution). Some sample distributions contributing to the population estimates were skewed. Therefore, it must be noted that the population standard deviations may be lower than those reported here, while the means are believed to be representative of the population. The recommended criteria were approximated from various source documents which specify weapons system and soldier performance requirements (US Army DCD, 1987; Headquarters, Dept. of the Army, 1988). These criteria are indicated in Figures 1 and 2 with an "*" and in Figures 3 and 4 with a "C". The criteria indicated in Figures 1-4 are arbitrary, and do not represent classified data.

Table 2
SHORAD Summary Performance Data

| _ | | | | |
|---|--|--|--|--|
| | I | ·W | RW | |
| SUMMARY PERFORMANCE MEASURES | ક | N | ક | N |
| Correctness of ID Hostiles Engaged Friends Engaged Engaged Aircraft Destroyed Hostile Attrition Friendly Fratricide Hostiles Releasing Ordnance | 75 77 39 92 72 35 62 | 49 37 37 33 31 31 37 | 85 81 23 85 76 19 83 | 57 57 57 41 41 41 41 |

Table 3 $\,$ FW Event Ranges (in kilometers) and Performance Outcomes by Intent

| | FRIENDLY | HOSTILE | OVERALL |
|-------|------------|------------|------------|
| | MEAN SD | MEAN SD | MEAN SD |
| RDET | 10.8 2.7 | 10.8 3.7 | 10.8 3.2 |
| RID | 5.7 2.2 | 6.0 2.4 | 5.8 2.3 |
| RLOCK | | 5.3 3.5 | |
| RFIRE | | 4.7 3.4 | |
| IDCOR | 72% | 79% | 75% |
| PKILL | <u> </u> | 72% | |
| | | | |

Table 4 $\,$ FW Event Ranges (in kilometers) and Performance Outcomes by Model Type

| FRIENDLY | | | | | | |
|--------------|--|--|--|--|--|--|
| F111 | | | | | | |
| EAN SD N | | | | | | |
| 3.4 4.0 18 | | | | | | |
| 4.9 3.0 18 | | | | | | |
| | | | | | | |
| | | | | | | |
| 59% | | | | | | |
| | | | | | | |
| | | | | | | |

| | 1 | HOSTILE | |
|-------|-------------|-------------|---------------|
| | SU24 | SU25 | MIG27 |
| | MEAN SD N | MEAN SD N | MEAN SD N |
| RDET | 11.3 4.4 18 | 10.7 3.5 35 | 10.5 3.1 61 |
| RID | 5.8 2.6 17 | 6.6 2.2 34 | 5.5 2.3 55 |
| RLOCK | | 4.6 3.4 14 | 6.0 3.6 25 |
| RFIRE | | 4.2 3.4 14 | 5.3 3.4 27 |
| IDCOR | 70% | 83% | 84% |
| PKILL | | 77% | 77% |

Table 5
RW Event Times (in seconds) and Performance Outcomes by Intent

| | FRIENDL | Y | HOSTIL | E | OVERAI | LL |
|-------|---------|-----|--------|-----|--------|-----|
| | MEAN | SD | MEAN | SD | MEAN | SD |
| TDET | 8.7 | 2.5 | 7.2 | 3.5 | 8.3 | 3.5 |
| TID | 8.6 | 4.1 | 5.4 | 3.0 | 7.0 | 3.5 |
| TFIRE | | | 2.8 | 2.6 | | |
| THAND | | | 5.2 | 3.7 | | |
| TTOT | | | 11.0 | 3.7 | | |
| IDCOR | 80% | 5 | 90 | ક | 85 | 5% |
| PKILL | | | 82 | 8 | | |

Table 6 $$\rm RW\ Event\ Times\ (in\ seconds)\ and\ Performance\ Outcomes\ by\ Model\ Type$

| | | FRIENDLY | |
|-------|--------------|---------------|---------------|
| | AH1 | UHl | CH3 |
| | MEAN SD N | MEAN SD N | MEAN SD N |
| TDET | 8.2 3.6 40 | 11.1 2.4 9 | 7.6 1.5 8 |
| TIO | 8.2 4.9 40 | 9.0 2.9 9 | 9.0 4.6 8 |
| TFIRE | 2.2 0.8 15 | | |
| THAND | 4.0 1.5 19 | | |
| TTOT | 12.4 6.5 21 | | |
| IDCOR | 77% | 87% | 75% |
| PKILL | 14% | | |

| | | HOSTILE | |
|-------|--------------|-------------|--------------|
| | MI8 | MI24 | MI28 |
| | MEAN SD N | MEAN SD N | MEAN SD N |
| TDET | 6.7 3.2 43 | 6.9 4.0 44 | 10.9 3.4 9 |
| TID | 5.4 3.1 40 | 5.0 3.3 41 | 5.7 2.0 9 |
| TFIRE | 2.3 1.6 39 | 3.3 3.0 41 | 2.4 3.3 9 |
| THAND | 4.8 2.9 44 | 5.3 4.1 44 | 9.4 6.3 9 |
| TTOT | 9.9 3.0 44 | 9.9 4.5 44 | 15.1 7.1 9 |
| IDCOR | 90% | 94% | 87% |
| PKILL | 88% | 77% | |

Figure 1
FW Engagement Event Sequence

Range in Fullscale Kilometers

| 1 | 2 | 3 | 4 * | 5 | 6 | 7 | 8 | 9 | 1ø | 11 | 12 | 13 |
|---------------------|------------|-------|-----|---|---|---|---|---|--------------|----|----|----|
| | Lock (5.3) | | | | | | | | Det 10.8) | | | |
| Fire ID (4.7) (5.8) | | | | | | | | | | | | |

* = Criterion

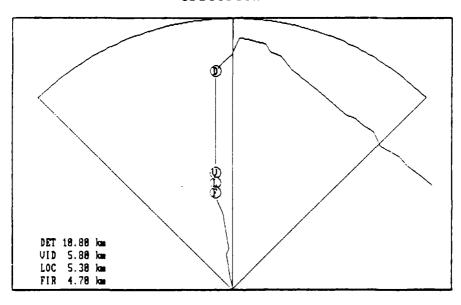


Figure 2 RW Engagement Event Sequence

Time in Seconds

| 24* | 22 | 2Ø | 18 | 16 | 14 | 12 | 10 | 8 | 6 | 4 | 2 | ø |
|-----|-----------------------|----|----|----|----|----|--------------|---|---|-----|---|---|
| | Lock (16.2) | | | | | (| Det (8.0) | | | | | |
| | Fire ID (19.0) (15.0) | | | | | | | | | Los | | |

* = Criterion

Distributions for FW Events (Kilometers)

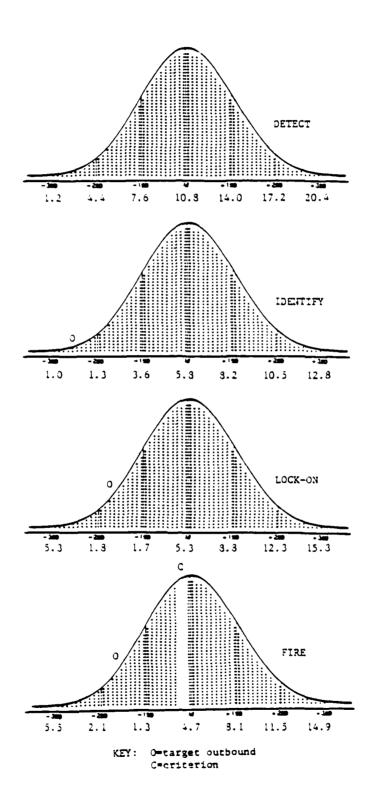


Figure 3

Distributions for RW Events (Seconds)

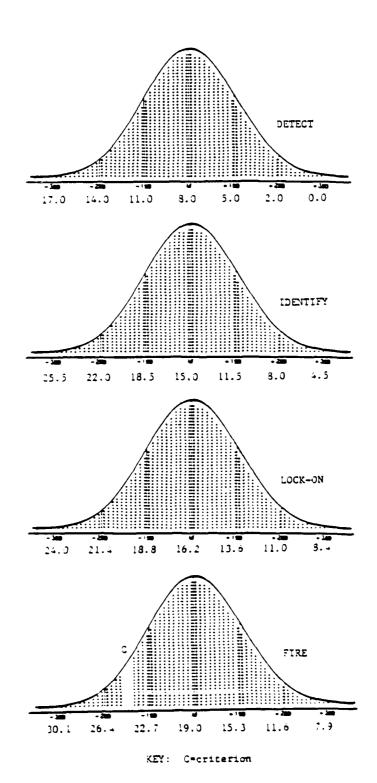


Figure 4

Consistency of Estimates with Full Scale Test Results: The parameter estimates presented were found to agree with data obtained from field tests conducted using full scale aircraft. Tables 7 through 10 present comparisons (when experimental conditions were similar enough to warrant a comparison) and demonstrate the consistency of RADES data with full scale field test data. Readers are also referred to the RADES Validation Report (Drewfs, Barber, Johnson, and Frederickson, 1988).

Conclusions: The purpose of the meta-analysis was to consolidate similar studies which investigated the same phenomena, in order to make generalizations about the SHORAD soldier population. The findings reported are assumed, for purposes of range table development, to be the best available approximation of the true population parameters based upon an aggregation of a series of RADES experiments (Barber, 1987).

A major conclusion of the meta-analysis was that the detection, identification, and acquisition of aircraft consume the majority of the engagement process. Improvements in detection and identification range and accuracy would result in major gains in overall SHORAD engagement efficiency and effectiveness. Some gains could also be found by selecting soldiers with superior vision, and providing the fire unit with accurate, timely, and consistent early warning and cuing information. Use of RADES or RTS for training and qualification testing and troop unit sustainment training would increase hostile attrition and fratricide avoidance at optimal ranges. This is because it enables soldiers to practice and master aircraft identification and engagement skills, against friendly and hostile targets, in a realistic range environment.

Another important conclusion was that many soldiers currently appeared to fall below the performance criteria for fixed wing engagements; only half the population met the criterion. Again, improvement could likely be acquired by reducing the time and increasing the range of detection, identification, and acquisition. While RW performance was consistently above criterion, the criterion failed to consider helicopter ordnance release prevention. Assuming an ordnance delivery time of 18 to 19 seconds for a helicopter popping-up and hovering at a range of 3 to 4 kilometers, half the population would be above and half below this adjusted criterion, indicating a situation similar to that found for fixed-wing.

It is also important to note that the meta-analysis only considered single target presentations, and did not cover the effects of multiple or sequential targets. Previous research in RADES has often shown poorer performance in conditions with multiple targets than in conditions with single targets.

Table 7
Fixed Wing Event Range Comparisons (in kilometers)-Wright (1966) versus RADES (1987)

| | RADES | WRIGHT | COMPARISON | 1 |
|------|------------|-------------------------|-------------------|---|
| VAR | Mean SD | N Mean N <u>t</u> - | value df 2-tailed | р |
| RDET | 10.8 3.2 5 | 2 10.0 27 1 | 1.05 77 p>.2 | |
| RID | 5.8 2.3 5 | 2 6.8 27] | 1.82 77 p>.05 | |
| | | | | |

NOTE: Assumes equal variances

Table 8 Fixed Wing Event Range Comparisons (in kilometers) for the A7 and Al0--Tillapaugh & Smith (1983) versus RADES (1987)

| | | | A7 | | | Α. | 10 | |
|-------|------------|--------|------|---------|------------------|--------|--------------------------------------|-----|
| VAR | <u>t</u> - | -value | df 2 | -tailed | p <u>t</u> -va | lue df | 2-taile | q f |
| RID | | 1.0 | 38 | p>.2 | Ø.1 | Ø 56 | p>.2 | |
| RFIRE | 1 | 1.5 | 38 | p>.2 | 2.3 | 1 49 | .01 <p<.0< td=""><td>05</td></p<.0<> | 05 |
| vom: | ~ | | | | | | | |

NOTE: RADES "fire" value based on data from hostile aircraft only

Table 9
Friendly Rotary Wing Event Time Comparisons (in seconds)-Lott (1977) versus RADES (1987)

| Time Interval | : Detection | to Identification | <u>-</u> |
|-----------------|-------------|-------------------|--------------|
| <u>t</u> -value | df | 2-tailed p | |
| 0.10 | 56 | p>.2 | - |

NOTE: Assumes equal variances

Table 10 Helicopter Event Time Comparisons (in seconds) for the AH1--CDEC (1978) versus RADES (1987)

| | RADES | HAT (3-4 km) HAT (2-6 km) |
|---------|----------------|---------------------------------|
| VAR | Mean SD N | Mean SD N Mean SD N |
| TDET | 8.2 3.6 40 | 5.5 8.1 24 10.5 9.1 32 |
| TID-DET | 8.2 4.9 40 | 6.5 12.1 24 6.0 8.6 32 |
| TID* | 16.4 4.9 40 | 16.0 12.7 24 16.5 11.6 32 |

^{*}Indicates time from line-of-sight to identification response

| | RADES vs. HAT | (3-4 km) | RADES vs. HAT (2-6 km) |
|---------|------------------------|-----------------------|--------------------------|
| VAR | <u>t</u> -value df 2 | 2-tailed p <u>t</u> | -value df. 2-tailed p |
| TDET | .89 62 | p>.2 | 1.4 7ð p>.1 |
| TID-DET | .79 62 | p>.2 | 0.25 70 p>.2 |
| TID* | .18 62 | p>.2 | 0.05 70 p>.2 |

^{*}Indicates time from line-of-sight to identification response

The final observation that warrants discussion relates to assessed aircraft kills. The rate of fratricide was somewhat high, and unacceptable to the friendly air community (19% and 35% in Table 2; 14% in Table 6). The attrition rate on hostiles was below the established limits (military standards require 75% and the achieved level was 60% to 70%). This reflects a need to include the requirement to discriminate friendly and hostile air elements in training as well as in qualification and certification testing.

Definition of Scenario Test Conditions

Requirement: To define live fire exercise (LFX) and engagement simulation exercise (ESX) test conditions and aircraft model inventory requirements needed for the proper administration of SHORAD training and qualification testing scenarios. Test conditions and aircraft model specifications must insure an equal probability of successful performance across weapons, crews, teams, and operators, within each particular difficulty level grouping of scenarios.

Procedures: Scenario test conditions were profiled for both engagement simulation and live fire test purposes. Differences in live fire range safety and testing procedures mandated that the two test conditions be specified separately. Draft test conditions specifications were then provided to ARI representatives for review and comment. Comments received back from ARI were then used to adapt the draft test conditions specifications.

Findings: Table 11 provides recommended specifications for test conditions, and Table 12 lists recommended aircraft model specifications for the LFX and ESX engagement range tables. While live fire specifications may change, given developments in live fire procedures, less change is expected in ESX test conditions specifications. Figure 5 presents the basic ESX range layout utilized during field tests associated with criteria development and validation efforts.

Scenario Scripting and Generation

Requirement: To establish a library of engagement qualification and training scenarios for use in administering the SHORAD range tables. The scenario library must be inclusive of a full range of factors known to alter SHORAD part-and whole-task performance difficulty (e.g., alerting and cuing, target size, target type, target number, and target intent).

Engagement Simulation (ESX)

- Sky Background
- Clear Day (20+ Miles Visibility)
- Stationary Weapon Position
- 90 degree Search Sector
- Unaided Detection
- Aided Recognition (binoculars)
- Cuing (+ or 15 degrees accuracy)
- Early Warning Voice Message (60 seconds prior to availability)
- Air Defense warning Red, WCS Tight
- IFF Return Unknown
- One RW Practice Trial
- No trial-by-trial Feedback (End of day feedback)
- No Visitors at Weapon Site
- Windspeed not to Exceed 25 MPH
- Randomized Scenario Order
- Standardized Scenario
 Set
- Standard Target Coloration
- Matched Target Sizes
- RW Range: Stinger = 2 to 5 Km; Chaparral = 2 to 5 Km; Vulcan/PIVADS = .5 to 1 KM
- FW Availability 20 to 30 Km
- FW Airspeed 80 to 100 MPH (1/5 Scale)
- 4-Hour Blocks

Live Fire (LFX)

- Sky Background
- Clear Day (20+ Miles Visibility)
- Stationary Weapon Position
- 90 degree Search Sector
- Unaided Detection
- Aided Recognition (binoculars)
- Cuing (+ or 15 degrees accuracy)
- Early Warning Voice Message (60 seconds prior to availability)
- Air Defense warning Red, WCS Free
- IFF Return Unknown
- One RW Practice Trial
- No trial-by-trial Feedback (End of day feedback)
- No Visitors at Weapon Site
- Windspeed not to Exceed 25 MPH
- Randomized Scenario
 Order
- Standardized Scenario Set
- Standard Target Coloration
- Matched Target Sizes
- RW Range: Stinger = 2 to 5 Km; Chaparral = 2 to 5 Km; Vulcan/PIVADS = .5 to 1 KM
- FW Availability 10.5 Km
- FW Airspeed 80 to 100 MPH (1/5 Scale)
- 2-Hour Blocks

Table 12 Recommended Aircraft

| FIXED | WING | ROTARY WING | | | |
|---|-------------|-------------------------------|------------|--|--|
| Friendly | Hostile | Friendly | Hostile | | |
| AlØ Thunderbolt A7 Corsair F16 Falcon F111 Strike-Bomber | SU24 Fencer | UH60 Blackhawk AH64 Apache | MI28 Havoc | | |

Targets that are "similar" in size

- A7 and F16 and SU25
- AlØ and MIG27 and SU17
- Flll and SU24
- UH6Ø and AH64
- CH3 and MI24 and MI28

Procedures: RADES scenario scripting software was used, along with the DBASE III Plus relational database management software package, to establish the initial set of 20 scenarios. Scenario scripts were then produced for a basic library of 200 scenarios. Given approval of the 200 scenarios by ARI, the 200 scenarios will be encoded for use in the RTS. The 20 baseline scenarios were used as the test stimulus in SHORAD range table tryout testing.

Findings: Appendix A provides the 200 developed scenarios for air defense range table qualification and training purposes. While these are draft scenarios, SAIC has taken considerable care to preserve the scenario goals of DOTD and ARI in their construction. In addition, an SAIC estimate of situational difficulty is provided in the table, which takes into consideration those factors shown by the RADES meta-analysis and recent field data collection efforts to affect performance and workload.

Summary and Task Performance Measures Definition

Requirement: To define summary performance measures (SPM) which discriminate qualified crew, team, and operator engagement performance from unqualified performance:

 Under a wide range of scenario difficulty conditions,

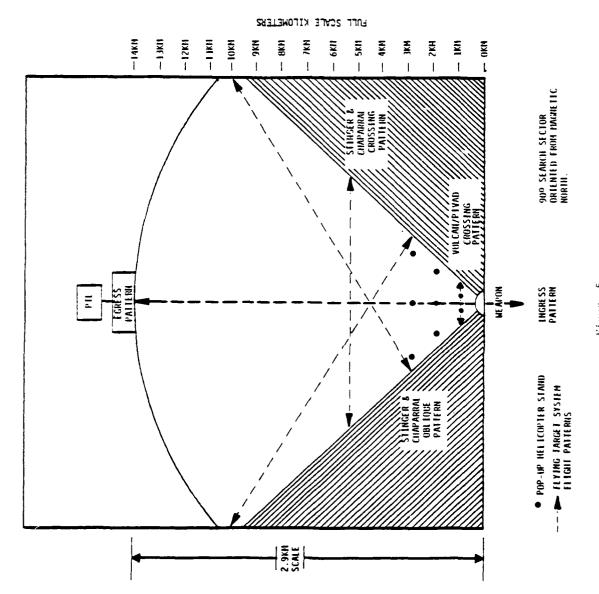


Figure 5 Range Layout

- Under a wide range of environmental conditions,
- Across the existing family of SHORAD weapon systems (i.e., Vulcan or PIVADS, Chaparral, and Stinger),
- Remaining sensitive to the individual differences of sub-groups of soldiers comprising the SHORAD soldier population.

A second requirement was to define part-task performance measures (TPM) which pointed to the sources of crew, team, or operator SPM failure, and which could be used validly, reliably, practically, and economically to assign corrective training actions:

- Across difficulty levels of scenarios,
- Across environmental conditions,
- Across the existing family of SHORAD weapon systems.

Procedures: SPM and TPM were selected if they had been shown in prior field test experiments to separate crews, teams, or operators on the basis of variation in performance. The measures sought were those sensitive to performance efficiency (speed, or TPM) or effectiveness (accuracy, or SPM), and of value in distinguishing between qualified and unqualified crews, teams, and operators. In addition, measures useful in diagnosing the sources of unqualified performance were also identified. In this regard, SPM and TPM which were selected demonstrated substantial variance. The ones that didn't were those for which performance was virtually perfect (95% or above), and they were not selected.

Table 13 lists all summary performance measures and definitions developed under the present research program. In addition, under LFX data collection operations, the SPM of number of rounds in the target area, mean hit point, and average miss distance, were integrated into the SPM set. Table 14 lists all task performance measures and definitions developed under the present research program. These candidate TPM and SPM were reduced after demonstrating which ones did not discriminate levels of achievement effectively.

Findings: What was sought in this analysis was maximum discrimination between groups on the basis of performance level. TPM which did not contribute to performance discrimination were dropped from further consideration. For example, fixed wing event response times were shown in prior RADES research applications to contribute little to the discrimination of high, medium, and low performers while fixed wing event ranges were extremely useful. Thus, only the event ranges were considered essential as FW TPM. The summary performance measures recommended for elimination were percent targets detected and percent aircraft identified. Both of these measures tended to exceed 95% in the RADES experiments conducted to date. variables should not be confused with "percent targets correctly identified", or "time and range of detection and identification" as these are among the most important measures studied within the present research effort. Further, the interrogation (IFF) event was found to be ineffective in discriminating achievement level, and was recommended for elimination from the criterion set. Instead, IFF was recommended for use as a teaching point, as this event should occur as soon as the target has been detected. Finally, the range and time of command to engage or cease engagement were found to correlate very highly with the identification event, so only the identification ranges and times were recommended for use as criteria.

Scoring Algorithm Development

Requirement: To establish a free-standing software package compatible with the Range Target System. The package must transform raw exercise data, calculate TPM and SPM scores, compare the calculated scores with TPM and SPM criterion cut-off values, and output hardcopy reports. Hardcopy reports must be produced for each respective crew, team, and operator, scenario performance difficulty level, and aircraft type class (RW or FW), such that only "like" scenarios scores are reported within any one hardcopy report for each crew.

Table 13
Candidate Summary Performance Measures (SPM)

| CODE | EVENT | DESCRIPTION | Dt | TY |
|--------|--------------------------------------|--|----|------|
| PDET | Proportion of Aircraft Detected | Number of detections divided by presentations | SL | & SG |
| PID | Proportion of Aircraft Identified | Number of identifications divided by presentations | | SL |
| IDCOR | Correctness of Identifications | Number of correct IDs divided by presentations | | SL |
| FIDCOR | Friendly Identifications | Number of correct IDs divided by presentations | | SL |
| HIDCOR | Hostile Identifications | Number of correct IDs divided by presentations | | SL |
| ENGAGE | Aircraft Engaged | Number of engagements divided by presentations | SL | & SG |
| FENG | Friendlies Engaged | Number of engagements divided by presentations | SL | & SG |
| HENG | Hostiles Engaged | Number of engagements divided by presentations | SL | & SG |
| FRAT | Friendly Fratricide | Number of friendly kills divided by presentations | SL | & SG |
| ATTRIT | Hostile Attrition | Number of hostile kills divided by presentations | SL | & SG |
| EFFECT | Engaged Aircraft Destroyed | Number of kills divided by engagements | SL | & SG |
| ORD | Hostiles Releasing Ordnance | Number of ordnance releases divided by hostile presentations | SL | & SG |

Table 14 Candidate Task Performance Measures (TPM)

| CODE | EVENT | DESCRIPTION | DUTY |
|-------|----------------|--|---------|
| | | | |
| | Detection | FW slant range at detection | SL & SG |
| RACQ | Acquisition | FW slant range at acquisition | SG |
| RIFF | Interrogation | FW slant range at interrogation | SG |
| RID | Identification | FW slant range at identify | SL |
| RENG | 1 | FW slant range at command engage or cease engagement | SL |
| RLOCK | Lock-on | FW slant range at lock-on | SG |
| RFIRE | Fire | FW slant range at fire | SG |
| RHAND | Hand-off | FW range interval from identify to fire | SL 2 SG |
| RTOT | Total | FW range interval from detect to fire | SL & SG |
| TDET | Detection | RW time interval from LOS to detection | SL & SG |
| TACQ | Acquisition | RW time interval from detect to acquire | SG |
| TIFF | Interrogation | RW time interval from detect to IFF | SG |
| TID | Identification | RW time interval from detect to identify | SL |
| TENG | | RW time interval from identify to command engage or cease engagement | SL |
| TLOCK | Lock-on | RW time interval from acquire to lock-on | SG |
| TFIRE | Fire | RW time interval from lock-on to fire | SG |
| DIAHT | Hand-off | RW or FW time interval from identify to fire | SL & SG |
| TOT | Total | RW or FW time interval from detect to fire | SL & SG |

Procedures: The research team employed RADES field test data as the example input. These files, containing raw field data from prior experiments, were fed into a prototype score calculation procedure. This resulted in associated $\ensuremath{\mathsf{TPM}}$ and $\ensuremath{\mathsf{SPM}}$ scoring outputs. Next, a pass-fail determination routine associated with SPM scores was generated, based on realistic qualification cut-off values. Then the TPM diagnostics calculation procedure was developed, which would indicate which TPM contributed most to whether SPM criteria were met or not. Utilities were added for the purposes of calculating scores for all crews associated with a multi-station test facility, specifically the multiple-weapon RADES configuration. New test data collected using the RADES testbed were brought in from the field on floppy disk, and fed into the newly-developed software scoring system to assess the degree of consistency with prior results. This was the final test and calibration step in the procedure for algorithm development.

Findings: After prototype development and testing, the scoring transformation algorithms and software implementing those algorithms were verified as operational. Table 15 provides the final score transformation algorithms and Table 16 depicts an example of the hardcopy report output for RW time data. Not shown in the algorithm figure is the filter used to deal with measures whose values are missing due to invalid engagement sequences, or equipment malfunctions. This software filter automatically prevents the miscalculation of scores due to missing values. (While the scoring system is currently written in DBASE III Plus command language, it is anticipated that this software will be either compiled into, or translated into, the "C" programming language in order to increase execution speed. That translation will be part of the RTS integration and demonstration program).

Scenario Feedback Display Definition

Requirement: To establish scenario-specific performance standards to be displayed as feedback which can be used in the sustainment training of SHORAD crews, teams, and operators. The scenario feedback display system is meant to be integrated into a field testing and sustainment training facility such as RADES or the RTS. It is currently anticipated that the feedback displays will not be used during SHORAD qualification and certification test exercises but will be used exclusively for training purposes. Use of the feedback displays in association with testing could alter the performance of tested crews, teams, or operators and result in invalidation of the performance standards.

Procedures: A modification of the previous RADES feedback display system (see Figures 6 and 7) was used as the prototype for future SHORAD training feedback. The major alteration made to this ARI-approved and field-tested display (not shown in figures) was the addition of task performance measure cut-off values (criteria), so that not only actual but required performance can be seen by the exercising soldiers and their instructors. These criterion values could then be compared easily to achieved soldier performance.

Findings: Figures 6 and 7 provide examples of the SHORAD crew, team, and operator feedback display. It is important to distinguish the feedback display, which is scenario-specific, from the scoring system and hardcopy reports, which cover all scenarios administered to a crew, team, or operator in the course of a qualification and certification test or training exercise. While feedback displays are generated one per trial for training purposes, hardcopy scoring reports are generated for training or test purposes, after several or all of the scenarios have been administered.

- If time of interrogation friend or foe greater than or equal to time of detection, transformed time of interrogation friend or foe equals time of interrogation minus time of detection.
- 2. If time of identification greater than or equal to time of detection, transformed time of identification equals time of identification minus time of detection.
- 3. If time of acquire greater than or equal to time of detection, transformed time of acquire equals time of acquire minus time of detection.
- 4. If time of command to engage greater than or equal to time of identification, transformed time of command to engage equals time of command to engage minus time of identification.
- 5. If time of command to cease fire greater than or equal to time of identification, transformed time of command to cease fire equals time of command to cease fire minus time of identification.
- 6. If time of lock-on greater than or equal to time of acquire, transformed time of lock-on equals time of lock-on minus time of acquire.
- 7. If time to superelevate is greater than or equal to time of command to engage, transformed time to superelvate equals time to superelevate minus time of command to engage.
- 8. If time of fire greater than or equal to time of lockon, transformed time of fire equals time of fire minus time of lock-on.
- 9. If time of fire greater than or equal to time of command to engage, transformed time of hand-off equals time of fire minus time of command to engage.
- 10. If time of re-attack (second fire) greater than or equal to time of fire, transformed time of re-attack equal time of re-attack minus time of fire.
- If time of kill greater than or equal to time of fire, transformed time of kill equal time of kill minus time of fire (i.e., round flight time). Round flight time computations were based on approximations of classified data to protect their sensitivity.

Table 16. Scoring Algorithm Output

FIXED WING SCENARIO: DIFFICULTY=HIGH

TASK PERFORMANCE MEASURES DIAGNOSTICS

| TPM | MEAN | STATUS | CRITERIA |
|----------------------|----------------|-----------------|----------|
| RANGE OF DETECTION | <u> 117</u> 68 | MEETS CRITERION | 8000 |
| RANGE OF ID | 3909 | BELOW CRITERION | 4000 |
| RANGE OF ACQUISITION | 3389 | BELOW CRITERION | 5000 |
| RANGE OF LOCK-ON | 2611 | BELOW CRITERION | 4000 |
| RANGE OF FIRE | 1760 | BELOW CRITERION | 2000 |

SPECIAL GUN SYSTEM LFX SCORES NUMBER OF ROUNDS ON TARGET

=

MEANS

MEANS

MISS DISTANCE HIT POINT

_

PASS-FAIL DETERMINATION

| | SPM | SCORE | STATUS | CRITERIA |
|----|---------------------|-------|---------|----------|
| ક | CORRECT ID | 100 | PASSING | 70 |
| 8 | AC DESTROYED | 100 | PASSING | 60 |
| É | FRIENDS ENG | Ø | PASSING | 3Ø |
| ક | HOSTILES ENG | 100 | PASSING | 75 |
| ક | FRIENDS CORRECT ID | 100 | PASSING | 70 |
| ક | HOSTILES CORRECT ID | 100 | PASSING | 75 |
| કે | FRATRICIDES | Ø | PASSING | 25 |
| કે | ATTRITION | 100 | PASSING | 45 |

SPECIAL GUN SYSTEM LFX SCORES

AVERAGE NUMBER OF ROUNDS ON TARGET =

AVERAGE NUMBER OF ROUNDS PER BURST =

AVERAGE NUMBER OF TARGETS KILLED =

CREW: 01 03/03/88 14:56:26

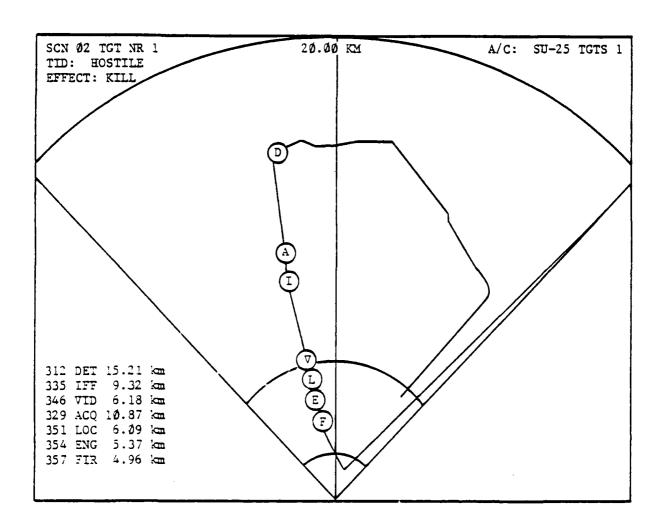


Figure 6
Fixed Wing Scenario Feedback Screen

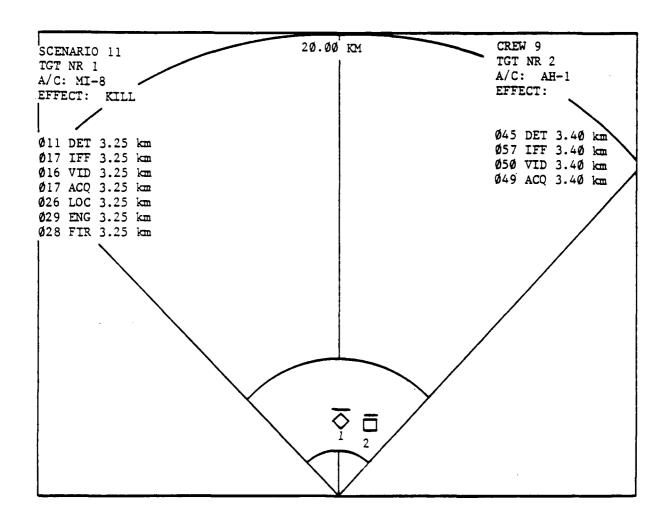


Figure 7
Rotary Wing Scenario Feedback Screen

Determination of Scenario Difficulty Factors

Requirement: To determine the difficulty of a scenario based on target, soldier, and environmental factors.

Procedures: Difficulty criteria were identified based on air defense research findings and the human factors literature. The level of difficulty criteria are given in Appendix B. Each difficulty factor was assigned a relative weight, based upon its expected effect on performance. Three sources of data were utilized for obtaining the difficulty scaling factors and ascribing relative weights to them. These were: subject matter experts, the available literature, and previous RADES data.

The difficulty level for each scenario in a standard set of 20, was derived by each expert judge, and across expert judges. Agreement among the experts was good regarding the factors considered important for establishing scenario performance difficulty levels. In rating the difficulty of the scenarios, interrater reliability was also good as demonstrated by Spearman correlations (range of r-values = .17 to .92; average r-value = .68, p < .001). Subject matter experts were members of the research team from ARI and SAIC.

Data (SPM and TPM) obtained from field test administrations of the standard set of scenarios were established as baseline parameters of performance. The difficulty criteria weights were then used to predict variations in performance. Performance variations were consistent with the difficulty criteria weights ascribed to the scenarios.

The method used to derive scenario difficulty scores was based on classic decision analysis logic. The process began with the identification of difficulty factors. These factors were ascribed relative weights by subject matter experts based on their evaluation of how performance was affected by the factors. Each factor was comprised of several subfactors which related to specific scenario conditions characteristic of the factors under which they were categorized. These subfactors were ascribed values, which, when multiplied by the associated factor weight, resulted in a difficulty score for that factor. The factor score was therefore dependent on the subfactor which was relevant to the scenario being scaled. A total difficulty score was derived for each scenario based on the sum of all difficulty scaling factor scores. Scenario difficulty levels (1 through 5, or low to high) were assigned to each scenario which reflected the relative differences between scenario difficulty scores.

Findings: Given that interrater reliability was good, ratings accounting for the highest variance in performance (R²) were employed to ascribe scenario difficulty. These difficulty predictor weights were subsequently used to assign performance difficulty levels to the 200 scenarios developed during this effort (See Appendix A).

Scenario Field Testing

Requirement: To subject the draft scenarios, scenario difficulty indices, task and summary performance measures, SPM and TPM cut-off values, test conditions, and scoring system to empirical test and evaluation on representative samples of soldiers and weapons.

Procedures: Ten Stinger teams from the Stinger Platoon, Headquarters and Headquarters Troop, Third Armored Cavalry Regiment stationed at Fort Bliss, Texas participated in the study. The test was conducted at White Sands Missile Range, White Sands, New Mexico, in desert terrain, in clear weather, under daylight conditions, during the month of January of 1988, using the RADES instrumented testbed. Each Stinger team was exposed to as many as twenty scenarios. Each scenario presented either flying, fixed-wing (FW) and/or pop-up, rotary-wing (RW) targets, either in single or multi-target presentations. Scenario specifications are provided in Table 17. The scenario sequences executed for each team are given in Table 18. Each Stinger team (consisting of a team chief and gunner) was given an early warning twenty seconds prior to each scenario presentation. Cuing information was not provided. Team chiefs were given binoculars, which they used for aircraft identification purposes only.

Task performance measures (TPM) included times and ranges associated with target detection, interrogation, acquisition, identification, lock-on, superelevation, and fire. Summary performance measures (SPM) included correctness of identification, engagement effectiveness (i.e., kill or miss), hostile attrition, hostile ordnance delivery prevention, and fratricide. Dependent variables used are listed and described in Table 19.

Table 17 Standardized Scenario Set

| SCEN NO. | TYPE | INTENT | AIRCRAFT | AZIMUTH | ASPECT | | PRESENT. ORDER | DUR. | LOD |
|-------------|------|--------|---------------|---------|---------|-------|-------------------|------|-----|
| 1 | FW | F | A10 | 12 | 0 | A | | | MH |
| 2 | FW | F | F16 | 1 | 45 | В | | | MH |
| 3 | FW | F | F111 | 10 | 90 | С | | ' | М |
| 4 | FW | Н | MIG27 | 12 | Ø | A | | | MH |
| 5 | FW : | н | SU25 | 11 | 45 | В | | | MH |
| 6 | FW | H | SU24 | 2 | 90 | С | · · | | M |
| 7 | RW | F | UH6Ø | 11 | 90 | 3 | | 25 | L |
| 8 | RW | F | CH3 | 12 | 45 | 5 | | 25 | ML |
| 9 | RW | Н | MI? (HOKUM) | 11 | 90 | 3 | | 25 | L |
| 10 | RW | н | MI8 | 12/11 | 45 | 7/5 | SEQUEN | 10 | ML |
| 11 | RW | н | MI24 | 12/1 | Ø | 5/3 | SEQUEN | 1Ø | L |
| 12 | RW | F | AH1/UH1 | 11/1 | 45 | 3 | SEQUEN | 25 | L |
| 13 | RW | Н | MI8/MI24 | 12/1 | 45 | 7/5 | SEQUEN | 25 | ML |
| 14 | RW | F/H | CH3/MI8 | 11/1 | 45 | 5 | SIMULT | 40 | ML |
| 15 | RW | H | MI8/MI28/MI24 | 11/12/1 | 45 | 3/5/5 | SIMULT | 50 | M |
| 16 | RW | F/H/H | AH1/MI24/MI28 | 11/12/1 | 90 | 3/7/5 | SIMULT | 40 | M |
| 17 | RW | F/H/F | CH3/MI28/UH1 | 11/12/1 | 45 | 5/5/3 | SIMULT | 40 | M |
| 18 | Both | F/H | A7/MI24 | 12/1 | 0/45 | A/3 | SIMULT | 3Ø | H |
| 19 | Both | н | SU17/MI?/MI28 | 11/12/1 | 45/45/0 | B/5/3 | SIMULT | 60 | Н |
| 20 | Both | H/F/H | SU25/UH60/MI8 | 12/11/1 | 0/45/45 | A/5/5 | SIMULT | 40 | Н |
| | | | | | | | | | |

Difficulty levels: H=high, M=medium, L=low

FW Patterns: A = ingress at Ø degrees aspect; B = diagonal ingress at 45 degrees aspect; C = crossing pattern at 90 degrees aspect

Table 18 Scenario Presentation Sequence

| TEAMS | SCENARIO SEQUENCE |
|---------|--|
| 1,2,3,4 | D,9,11,13,18,10,3,8,16,2,20,5,14,7,6,15,4,17,1,12 |
| 5,6,7 | D,15,7,14,17,4,11,5,12,20,8,6,16,18,3,9,10,1,13,19,2 |
| 8,9,10 | D,1,12,10,9,2,13 |

KEY: D = Dummy or practice trial

Table 19 Dependent Variables

| CODE | TITLE or DESCRIPTION | DUTY | INTERPRETATION |
|--------|----------------------------------|----------|---|
| IDCOR | Correctness of Identification | TL | Number of correct identifications divided by number of targets identified |
| FIRED | Weapon Fired | G | Number of weapon fires divided by number of targets presented. |
| EFFECT | Target Hit or Missed | 3 | Number of targets killed divided by number engaged |
| FRAT | Fratricide | вотн | EFFECT on Friendlies |
| ATTRIT | Attrition | ВОТН | EFFECT on Hostiles |
| ORD | Ordnance Prevention | вотн | Number of hostiles delivering ordnance divided by number presented |
| RDET | Range of Detection | TL or G | The slant range from the weapon to the target when the |
| RID | Range of Identification | TL | event took place; greater ranges usually indicate |
| RACQ | Range of Initial Acquisition | G | better performance for detection and identification but not always for the |
| RIFF | Range of Interrogation | G | other events (target can be inbound or outbound). Range is relevant for |
| RLOCK | Range of Lock-on | G | fixed-wing targets only since rotary- wing targets simply |
| RFIRE | Range of Weapon Fire | G | pop-up from a static position. Ranges are in full scale kilometers. |

Table 19 (Continued) Dependent Variables

| CODE | TITLE or DESCRIPTION | YTUD | INTERPRETATION |
|-------|--------------------------------|---------|--|
| TDET | Time of Detection | TL or G | Based on seconds after target availability; availability begins when visual line-of-sight is achieved on the first RW target |
| TID | Time of Identification | TL | Time interval between Detection and Identification |
| TACQ | Time of Initial Acquisition | G | Time interval between Detection and Acquisition |
| TIFF | Time of Interrogation | G | Time interval between Detection and IFF |
| TLOCK | Time of Lock-On | G | Time interval between Acquisition and Lock-On |
| TFIRE | Time of Weapon Fire | G | Time interval between Lock-On and Fire |
| TTOT | Total Engagement Time | вотн | Time interval between Detection and Fire |
| THAND | Time of Handoff | нтов | Time interval between Command to Engage and Weapon Fire |

KEY: TL = Team Leader; G = Gunner

Findings: Table Cl (See Appendix C) depicts the average performance, number of cases, and the variability (standard deviation) across teams for each scenario. These data will be used as a benchmark in estimating future performance on this same set of 20 scenarios, or an equivalent sample of like-difficulty scenarios. It is anticipated that future performance on these scenarios will be approximately equal for soldiers with similar experience and ability, and that performance will fall within reasonable boundaries (90 percent confidence interval) established in this table. Data contained in Table Cl are self explanatory and therefore require no detailed elaboration here.

Tables 20 and 21 provide the summary performance of soldiers according to scenario conditions across all observations. As shown in Table 20, soldiers accurately identified friendly helicopters 45% of the time and hostile helicopters 71% of the time. Friendly FW were accurately identified 69% and hostile FW 85% of the time. The friendly fixed wing F-16 and the friendly rotary wing CH-3 were frequently misidentified. Attrition rates on hostile aircraft were 70% for FW and 41% for RW.

Further, performance effectiveness (identification correctness: IDCOR; and engagement effect: EFFECT) decreased in multiple RW target scenarios (See Table 21). Identification accuracy and engagement effectiveness (EFFECT, ATTRIT, and ORD) decreased with increased workload. Thus, aircraft model type, intent, and the number of targets (workload level), were deemed important factors for assessing scenario difficulty level.

Table 22 shows the relationship between RW elevation, offset from PTL, and presentation aspect on measures of engagement performance. Data are summed over all teams and targets for all relevant scenarios. Improved target visibility, as measured by RW target elevation, offset, and aspect, resulted in improved performance on both TPM and SPM. Target visibility was a major factor used in assessing scenario difficulty. See also Table Cl for information on how performance varied in terms of target range, aspect, and model type.

Tables 23 and 24 present the results of statistical analyses which show that observed engagement performance varied as a function of scaled scenario difficulty level. Difficulty level weights were assigned to scenarios by subject matter experts according to criteria known to affect engagement performance, such as target visibility, workload, intent, range, and model type. (See Appendix B). Generally, on more difficult scenarios, troops required more time for target identification, they locked onto and fired at identified hostile targets later, and they required more time for a complete engagement (detect to fire).

Table 20 Summary Performance Results by Target Type and Intent

| VARIABLE | TYPE | INTENT | MEAN | SD | N |
|----------|------|----------|------|-------------|-----|
| IDCOR | FW | Friendly | .69 | .47 | 26 |
| | FW | Hostile | .85 | .36 | 27 |
| | FW | Both | .77 | .46 | 53 |
| | RW | Friendly | .45 | . 5Ø | 62 |
| | RW | Hostile | .71 | .46 | 133 |
| | RW | Both | .62 | .49 | 195 |
| | Both | Both | .66 | .48 | 248 |
| FRAT | FW | Friendly | .08 | . 27 | 26 |
| | RW | Friendly | .32 | .47 | 62 |
| | Both | Friendly | . 25 | .44 | 88 |
| ATTRIT | FW | Hostile | .70 | .47 | 27 |
| | RW | Hostile | .41 | .49 | 131 |
| | Both | Hostile | .46 | .50 | 158 |

NOTE: Data are based on all applicable scenarios and teams.

Table 21 Summary Performance Results by Each Subsequent RW Target Worked

| VARIABLE | TARGET | MEAN | SD | N |
|----------|--------------------|-------------------|-------------------|-----------------------|
| IDCOR | 1 | .72 | .45 | 138 |
| | 2 | .62 | .49 | 80 |
| | 3 | .43 | .50 | 30 |
| | 411 | .66 | .48 | 248 |
| EFFECT | 1 2 3 All | .77 .58 .33 | .43 .50 .49 | 81 48 14 144 |
| FRAT | 1 | .62 | .42 | 59 |
| | 2 | .40 | .5Ø | 20 |
| | 3 | .11 | .33 | 9 |
| | All | .25 | .44 | 88 |
| ATTRIT | 1 | .62 | .49 | 79 |
| | 2 | .34 | .48 | 58 |
| | 3 | .19 | .40 | 21 |
| | All | .46 | .50 | 158 |
| ORD | 1 | .57 | .50 | 79 |
| | 2 | .97 | .18 | 60 |
| | 3 | .95 | .22 | 21 |
| | All | .77 | .42 | 160 |

NOTE: Data are based on all applicable scenarios and teams (excluding second target of sequential target scenarios).

Table 22 Effects of RW Scenario Variations on Performance (Significant Pearson Correlations)

| INDEPENDENT VARIABLE | DEPENDENT VARIABLE | CORR. | Ŋ | PROB. |
|---|---------------------------------------|-----------------------------|---------------------------------|--------------------------------------|
| RW Elevation Above Mask (.5 to 3.5 degrees; mean = 1.5) | TDET TID* TTOT EFFECT ORD | 33 34 19 15 28 | 173 168 115 114 179 | .000 .000 .019 .057 |
| RW Offset From PTL (1 to 55 degrees; mean = 15.2) | TDET TID* TID TACQ TTOT | .18 .22 .16 .21 | 164 160 159 133 109 | .009 .003 .019 .007 .022 |
| RW Aspect/ Orientation (0, 45 or 90 degrees) | TDET TID TLOCK IDCOR ORD | 13 12 15 .12 12 | 174 171 116 195 195 | .040 .067 .052 .050 |

 $[\]star$ = Raw TID; time from availability to ID. N = Number of RW target presentations.

Table 23 Results of \underline{t} Test Comparisons of Performance by Difficulty Level (Two-Tailed Test Using Separate Sample Variances)

| COME | PARI | SON | TYPE | VARIABLE | MEAN | SD | N | Т | DF | PROB |
|------|------------|-----|------|-------------------|-----------|----------|-------|-----|------|------|
| | | | | | | | | | | |
| ιi | √ 3 | M | FW | TID | 21.9;13.0 | 11.7;3.6 | 16;14 | 2.9 | 18.2 | .009 |
| H | ٧s | M | FW | RLOCK | 3.7; 5.7 | 1.7;0.5 | 10; 9 | 3.5 | 10.4 | .006 |
| Н | ٧s | M | FW | RFIRE | 3.0; 5.8 | 1.4;0.6 | 11; 8 | 5.9 | 13.7 | .000 |
| H | ٧s | .ฑ์ | FW | TTOT | 29.2;20.5 | 12.9;3.8 | 11; 8 | 2.1 | 12.3 | .056 |
| MΗ | ٧s | M | FW | TID | 17.2;13.0 | 6.5;3.6 | 20;14 | 2.4 | 30.8 | .024 |
| MН | vs | M | FW | RLOCK | 4.3; 5.7 | 1.9;0.5 | 10; 9 | 2.1 | 10.2 | .058 |
| ΜH | ٧s | M | FW | RFIRE | 3.8; 5.8 | 2.1;0.6 | 10; 8 | 2.8 | 10.6 | .017 |
| МΗ | ٧s | M | FW | ${f T}{f C}{f T}$ | 25.3;20.5 | 7.7;3.8 | 10; 8 | 1.7 | 13.6 | .108 |
| M | ٧s | L | RW | TTOT | 11.1; 8.9 | 3.8;3.8 | 37;20 | 2.1 | 39.0 | .046 |
| MН | VS | M | 3oth | TID | 17.2; 7.1 | 6.5;4.4 | 20;70 | 6.5 | 24.3 | .000 |
| MH | ٧s | M | Both | TCTT | 25.3;11.8 | 7.7;5.8 | 10;49 | 5.2 | 11.1 | .000 |
| МH | v.s | ML | Both | TΙυ | 17.2; 5.6 | 6.5;2.6 | 20;49 | 7.7 | 21.6 | .000 |
| MН | VS | ML | Both | ${f TTOT}$ | 25.3;11.1 | 7.7;3.8 | 10;37 | 5.7 | 10.2 | .000 |
| Н | VS | M | Both | TID | 12.8; 7.1 | 11.5;4.4 | 37;7Ø | 2.9 | 41.7 | .006 |
| Н | ٧s | Μ | Both | TFIRE | 4.5; 2.5 | 5.3;1.9 | 29;43 | 2.0 | 32.9 | .054 |
| Н | ٧s | M | Both | TTOT | 19.9;11.8 | 12.8;5.8 | 29;49 | 3.2 | 34.8 | .003 |
| | | | | | | | | | | |

N = Number of applicable FW or RW target presentations.

Table 24
Relationship Between Difficulty Level and Performance (Significant Kendall and Spearman Correlations)

| TYPE | DEPENDENT VARIABLE | KENDALL'S | N PRO | B SPEARMAN'S | N | PROB |
|----------------|------------------------------|------------------------|--|------------------|---------|------------------------------|
| FW FW FW | TID RFIRE TTOT FRAT | .85 91 54 .80 | 9 .00 4 .03 6 .07 5 .03 | 35 95 '5 74 | 9 4 6 5 | .000 .026 .046 .023 |

N = Number of Stinger teams for which applicable data were available.

There were exceptions to the above. For example, a scenario with a crossing FW pattern was determined to be easier than one with an ingressing FW pattern because the target was easier to detect and identify, and was more frequently identified correctly. However, it was also available for a shorter period of time, forcing the soldiers to complete the engagement sooner. Further, although more workload implied more difficulty, sometimes it resulted in shorter engagement times since the soldiers were rushed. Therefore, both an easy and a difficult scenario was characterized by shorter engagement times, depending upon the conditions. Increasing the number of targets often resulted both in higher hostile attrition rates and higher fratricide rates, since the soldiers were inclined to engage everything that appeared to pose a threat. As a rule, however, increases in difficulty resulted both in decreased engagement efficiency and decreased engagement effectiveness.

Scenario difficulty in this study, as measured by performance effectiveness and efficiency, was primarily attributed to:

- Target characteristics
 - Model Size
 - Intent
 - Type (RW versus FW)
- Visibility conditions
 - Target Elevation
 - Target Offset
 - Target Aspect
 - Target Speed
- Workload level
 - Number of Targets

This test empirically validated many of the difficulty factors used by the experts to ascribe weights to scenarios. Studies such as this enable researchers to estimate the difficulty of air defense scenarios from empirical evidence. The difficulty scaling technique used to assess the difficulty level of the 200 scenarios presented in Appendix A was based upon this empirical evidence.

Determination of SPM and TPM Cut-off Scores

Requirement: To establish SPM score cut-off values which sort SHORAD crews, teams, and operators into qualified and unqualified groups. It was required that SPM cut-off values be achievable, valid, reliable, practical, and economic to administer. A second requirement was to establish TPM score cut-off values which identified deficient part-task performance and which indicated the sources of failure to qualify.

Procedures: It was acknowledged from the onset of the present research that only the USAADASCH, Directorate of Training and Doctrine (DOTD), Fort Bliss, is chartered to, and proponent for, setting range qualification standards. Therefore the present research was limited to analysis, interpretation, and recommendation of SPM and TPM cut-off scores.

Analysts examined the results of the RADES meta-analysis, field test data, literature on threat and friendly air operations, airspace management, command, control and communications, and weapons capabilities and limitations. Then analysts assisted ARI in establishing realistic SPM cut-off scores, and in adapting the draft training and qualification scenarios to the current tactical Short Range Air Defense picture. It must be noted that data from the Vulcan or PIVADS weapons were not available. It was therefore assumed that the criteria would need to be adjusted to accommodate close-range weapons such as these.

Draft cut-off scores were subjected to empirical field testing using the RADES testbed. The field tests were conducted to insure that the current SHORAD soldier population could attain the performance standards, and that those standards could be reliably, practically, and economically administered. The Stinger test described earlier helped to serve this purpose, and verified that these requirements were met.

Findings: Table 25 provides the recommended SPM cut-off scores established by the present program of research. Table 26 provides the recommended TPM cut-off scores which are to be used in diagnosing the sources of crew, team, and operator failures to qualify on SPM. It should be noted that all TPM ranges reflect incoming (not outgoing) FW targets.

Table 25
SPM Cutoff Values Estimated From RADES Research Results

| | FIXED WI | ING | ROTARY WING | | | |
|------------------------------|-------------|-------------------|------------------------------------|-------------|-------------------|--|
| SPM | LOD | VALUE | SPM | LOD | VALUE | |
| Identity | H | 70% | Identity | H | 7Ø% | |
| Correctness | M | 75% | Correctness | M | 75% | |
| (IDCOR) | L | 80% | (IDCOR) | L | 8Ø% | |
| Friends Identified (FIDCOR) | H M L | 70ቴ 75ቴ 80ቴ | Friends Identified (FIDCOR) | H M L | 7Øቄ 75ቄ 8Øቄ | |
| Hostiles Identified (HIDCOR) | H M L | 75% 80% 85% | Hostiles Identified (HIDCOR) | H M L | 75% 8Ø% 85% | |
| Friends | H | 30% | Friends | H | 30% | |
| Engaged | M | 25% | Engaged | M | 25% | |
| (FENG) | L | 20% | (FENG) | L | 20% | |
| Hostiles | H | 75% | Hostiles | H | 75% | |
| Engaged | M | 80% | Engaged | M | 80% | |
| (HENG) | L | 85% | (HENG) | L | 85% | |
| Friendly Kills (FRAT) | H M L | 25% 20% 15% | Friendly Kills (FRAT) | H M L | 25% 20% 15% | |
| Hostile | H | 45% | Hostile | H | 55% | |
| Kills | M | 60% | Kills | M | 70% | |
| (ATTRIT) | L | 75% | (ATTRIT) | L | 80% | |
| Engaged/ | H | 60% | Engaged/ | H | 75% | |
| Destroyed | M | 75% | Destroyed | M | 85% | |
| (EFFECT) | L | 90% | (EFFECT) | L | 95% | |
| Ordnance | H | 95% | Ordnance | H | 95% | |
| Released | M | 75% | Released | M | 75% | |
| (ORD) | L | 30% | (ORD) | L | 30% | |

LOD = Level of Difficulty

Table 26
TPM Cutoff Values Estimated From RADES Research Results

| | FIXED WI | NG | ROT | PARY WING | 3 |
|--------------------|-------------|------------------------------|-------------------|-------------|---------------------------------|
| TPM | LOD | VALUE | TPM | LOD | VALUE |
| Detect (RDET) | H M L | 8.0 km 11.0 km 14.0 km | Detect (TDET) | H M L | 10.0 sec 6.0 sec 4.0 sec |
| Acquire (RACQ) | H M L | 5.0 km 6.0 km 7.0 km | Acquire (TACQ) | H M L | 6.0 sec 5.0 sec 4.0 sec |
| Identify (RID) | H M L | 4.0 km 6.0 km 8.0 km | Identify (TID) | H M L | 9.0 sec 7.0 sec 5.0 sec |
| Engage (RENG) | H M L | 3.5 km 5.5 km 7.5 km | Engage (TENG) | H M L | 2.0 sec 1.0 sec 1.0 sec |
| Lock-On (RLOCK) | H M L | 4.0 km 5.0 km 6.0 km | Lock (TLOCK) | H M L | 6.0 sec 4.0 sec 2.0 sec |
| Fire (RFIRE) | H M L | 2.0 km 4.0 km 5.0 km | Fire (TFIRE) | H M L | 5.0 sec 3.0 sec 2.0 sec |
| LOD = Level | of Diff | ficulty | Total (TTOT) | H M L | 15.0 sec 12.0 sec 8.0 sec |

It can be seen, when comparing the Stinger test results cited earlier (Table Cl and Table 20) to the criteria established a-priori (Tables 25 and 26) that soldiers met some of the criteria but failed to meet others. For example, while correctness of target identification was often within tolerance limits, ordnance prevention and fratricide rates often were not. This is consistent with the observation made earlier that many of the system and operator performance standards were not currently being achieved. This may be due in part to the fact that the TPM and SPM estimates were based on cued trials, and the Stinger test results were based on non-cued trials. The decision to base the criteria on cued trials was reached after the Stinger test was conducted. Overall, however, the Stinger test results cited earlier were consistent with the TPM and SPM estimates. example, event ranges for moderately difficult FW scenarios for detection, identification, acquire, and fire were estimated at about 11, 6, 6, and 4 kilometers, respectively. These estimated ranges were similar to those obtained in the Stinger test. Further, these events for low difficulty RW scenarios were estimated at about 4, 5, 4, and 2 seconds, respectively. Again these estimated values were consistent with performance in the Stinger test.

SPM and TPM cut-off scores were determined as a function of scenario difficulty. Definition of meaningful SPM cutoff levels was accomplished as a natural by-product of the meta-analysis, and the RADES experiment described earlier. TPM cut-off scores were established in the same way. It is currently anticipated, however, that TPM cut-off scores will be used solely for diagnosing the sources of SPM failures to qualify, and will not be the basis for crew, team, or operator pass or fail determinations.

REFERENCES

- Barber, A. V. (1987). The Realistic Air Defense Engagement System: Three years of research results. El Paso, TX: Science Applications International Corporation.
- Drewfs, P. R., Barber, A. V., Johnson, D. M., & Frederickson, E. W. (1988). Validation of the Realistic Air Defense Engagement System (RADES). (ARI Technical Report 789). Alexandria, VA: U.S. Army Research Institute for the Behavioral and Social Sciences.
- Headquarters, Dept. of the Army (1988). Standards in weapons training. (DA PAM 350-38). Washington, DC: U.S. Army.
- Lott, T. (1977). Independent evaluation of the Stinger weapon system. Falls Church, VA: U.S. Army Operational Test and Evaluation Agency.
- Tillapaugh, C., & Smith, P. (1983). Stinger-Post man portable air defense system operational test II. Falls Church, VA: U.S. Army Operational Test and Evaluation Agency.
- U.S. Army Combat Developments Experimentation Command (1978).

 Helicopter acquisition test (HAT) (CDEC #FC094). Fort Ord,

 CA: CDEC.
- U.S. Army Directorate of Combat Developments (1987). Capstone required operational capabilities for the Forward Area Air Defense (FAAD) System(s): Annex H-Line-of-Sight Forward Heavy (LOS-F-H) component, FAADS. Ft. Bliss, TX: US Army Air Defense Artillery School (USAADASCH).
- Wright, A. D. (1966). The performance of ground observers in detecting, recognizing, and estimating range to low-altitude aircraft (Humrro Technical Report No. 66-19). Alexandria, VA: George Washington University.

APPENDIX A

RTS SCENARIO LIBRARY AND TARGET SPECIFICATIONS

| Scen | No. | m | | Aircraft | | | | | Seconds | |
|------|------|------|--------|----------|---------|--------|--------|--------|-----------|-------|
| No. | rarg | rype | Intent | woder | Azimuth | Aspect | /Stand | Order | Avaii. | rever |
| 1 | 1 | FW | F | 1 | 10 | 90 | A | | | M |
| 2 | ī | FW | F | ī | 11 | 45 | В | | | MH |
| 3 | 1 | FW | F | 1 | 12 | Ø | C | | | MH |
| 4 | 1 | FW | F | 1 | 1 | 45 | D | | | MH |
| 5 | 1 | FW | F | 1 | 2 | 90 | E | | | M |
| 6 | 1 | FW | F | 2 | 10 | 90 | Α | | | M |
| 7 | 1 | FW | F | 2 | 11 | 45 | В | | | MH |
| 8 | 1 | FW | F | 2 | 12 | Ø | C | | | MH |
| 9 | 1 | fw | F | 2 | 1 | 45 | D | | | MH |
| 10 | 1 | FW | F | 2 | 2 | 90 | E | | | M |
| 11 | 1 | FW | F | 3 | 10 | 90 | Α | | | M |
| 12 | 1 | FW | F | 3 | 11 | 45 | В | | | MH |
| 13 | 1 | PW | F | 3 | 12 | Ø | C | | | MH |
| 14 | 1 | FW | F | 3 | 1 | 45 | D | | | MH |
| 15 | 1 | FW | F | 3 | 2 | 90 | E | | | M |
| 16 | 1 | F₩ | H | 4 | 10 | 90 | A | | | M |
| 17 | 1 | fw | н | 4 | 11 | 45 | В | | | MH |
| 18 | 1 | FW | H | 4 | 12 | Ø | C | | | MH |
| 19 | 1 | FW | Н | 4 | 1 | 45 | D | | | MH |
| 2Ø | 1 | ew | H | 4 | 2 | 90 | Ε | | | M |
| 21 | 1 | FW | H | 5 | 10 | 90 | A | | | M |
| 22 | 1 | ew | H | 5 | 11 | 45 | В | | | MH |
| 23 | 1 | FW | Н | 5 | 12 | Ø | С | | | MH |
| 24 | 1 | FW | Н | 5 | 1 | 45 | D | | | MH |
| 25 | 1 | FW | H | 5 | 2 | 90 | E | | | М |
| 26 | 1 | FW | Н | 6 | 10 | 90 | A | | | M |
| 27 | 1 | FW | Н | 6 | 11 | 45 | В | | | MH |
| 28 | 1 | FW | H | 6 | 12 | Ø | С | | | MH |
| 29 | 1 | FW | Н | 6 | 1 | 45 | D | | | MH |
| 3Ø | 1 | fw | H | 6 | 2 | 90 | ε | | | M |
| 31 | 2 | FW | F | 1,2 | 11 | 45 | В | Sequen | | н |
| 32 | 2 | FW | F | 2,3 | 11,12 | 45,0 | D,C | Sequen | | H |
| 33 | 2 | FW | F | 3 | 12 | Ø | C | Sequen | | H |
| 34 | 2 | FW | Н | 4,5 | 1 | 45 | В | Sequen | | H |
| 35 | 2 | FW | Н | 5,6 | 11,12 | 45,0 | D,C | Sequen | | H |
| 36 | 2 | FW | H | 6 | 12 | Ø | С | Sequen | | H |
| 37 | 2 | FW | F,H | 3,6 | 11,1 | 45 | B,D | Sequen | | H |
| 38 | 2 | FW | H,F | 6,3 | 1,11 | 45 | D,B | Sequen | | H |
| 39 | 2 | fW | F,H | 2,4 | 12 | Ø | С | Sequen | | H |
| 40 | 2 | FW | H,F | 4,2 | 1 | 90 | E | Sequen | | MH |
| 41 | 2 | fw | F | 1 | 12 | Ø | C | Simult | | MH |
| 42 | 2 | FW | H | 5 | 12 | Ø | C | Simult | | MH |
| 43 | 2 | FW | F | 1,3 | 12,2 | 0,90 | C,E | Simult | | ХH |
| 44 | 2 | FW | F | 2 | 10,12 | 90,0 | A,C | Simult | | ХH |
| 45 | 2 | FW | Н | 4,6 | 12,2 | 0,90 | C,E | Simult | : | ХH |

| Scen | No. | _ | | Aircraft | Clock | Degrees | Pattern | Pres. | Seconds | Diffic |
|----------|--------|----------|--------|----------|---------|----------|---------|--------|----------|--------|
| No. | Targ | Type | Intent | Model | Azimuth | Aspect | /Stand | Order | Avail. | Level |
| 46 | 2 | FW | H | 4 | 10,12 | 90,0 | A,C | Simult | | хн |
| 47 | 2 | FW | F,H | 2,5 | 11,1 | 45 | B,D | Simult | | ХH |
| 48 | 2 | FW | H,F | 6,1 | 10,2 | 90 | A,E | Simult | | ХH |
| 49 | 2 | FW | F,H | 2,5 | 10,11 | 90,45 | A,B | Simult | | хн |
| 5Ø | 2 | FW | H,F | 6,1 | 1,2 | 45,90 | D,E | Simult | | ХH |
| 51 | 1 | RW | F | 11 | 11 | 45 | i | | 25 | L |
| 52 | 1 | RW | F | 11 | 12 | 90 | 4 | | 25 | L |
| 53 | 1 | RW | F | 11 | 1 | Ø | 5 | | 25 | L |
| 54 | 1 | RW | F | 11 | 1 | 45 | 6 | | 25 | ML |
| 55 | 1 | RW | F | 12 | 11 | Ø | 1 | | 25 | L |
| 56 | 1 | RW | F | 12 | 11 | 90 | 1 | | 25 | L |
| 57 | 1 | RW | F | 12 | 12 | 45 | 3 | | 25 | L |
| 58 | 1 | RW | F | 12 | 1 | 45 | 6 | | 25 | ML |
| 59 | 1 | RW | F | 13 | 11 | 45 | 2 | | 25 | ML |
| 60 | 1 | RW | F | 13 | 12 | 45 | 4 | | 25 | ML |
| 61 | 1 | RW | F | 13 | 1 | Ø | 5 | | 25 | L |
| 62 | 1 | RW | F | 13 | 11 | 90 | 6 | | 25 | L |
| 63 | 1 | RW | F | 14 | 11 | Ø | 2 | | 25 | ML |
| 64 | 1 | RW | F | 14 | 12 | 45 | 3 | | 25 | L |
| 65 | 1 | RW | F | 14 | 12 | 90 | 4 | | 25 | ML |
| 66 | 1 | RW | F | 14 | 1 | 45 | 5 | | 25 | L |
| 67 | 1 | RW | H | 15 | 11 | 45 | 1 | | 25 | L |
| 68 | 1 | RW | H | 15 | 11 | 45 | 2 | | 25 | ML |
| 69 | 1 | RW | Н | 15 | 12 | Ø | 3 | | 25 | L |
| 70 | 1 | RW | H | 15 | 1 | 90 | 6 | | 25 | L |
| 71 | 1 | RW | H | 16 | 11 | Ø | 1 | | 25 | L |
| 72 | 1 | RW | H | 16 | 12 | 45 | 3 | | 25 | L |
| 73 | 1 | RW | H | 16 | 12 | 90 | 4 | | 25 | L |
| 74 | 1 | RW | H | 16 | ,1 | 45 | 6 | | 25 | ML |
| 75 76 | 1 | RW | H | 17 | 11 | 45 | 1 | | 25 | L |
| 76 | 1 | RW | H | 17 | 12 | 0 | 3 5 | | 25 25 | L |
| 77 78 | 1 1 | RW | H | 17 17 | 1 1 | 45 9ø | 5 6 | | 25 25 | L L |
| 79 | 1 | RW RW | H H | 18 | 11 | 90 90 | 2 | | 25 | L |
| 80 | i | RW | п Н | 18 | 11 | 45 | 2 | | 25 | ML |
| 81 | i | RW | H | 18 | 12 | 45 | 4 | | 25 | ML |
| 82 | i | RW | H | 18 | 1 | ø | 5 | | 25 | L |
| 83 | 2 | RW | F | 11 | 12 | Ø | 4,2 | Seguen | | L |
| 84 | 2 | RW | F | 13 | 12,1 | 90 | 4,6 | Sequen | | Ĺ |
| 85 | 2 | RW | F | 14 | 11,12 | 45 | 1,4 | Sequen | | L |
| 86 | 2 | RW | F | 13,12 | 1,11 | 45 | 6,1 | Sequen | | Ĺ |
| 87 | 2 | RW | H | 15 | 11 | ø | 1,2 | Sequen | | ī. |
| 88 | 2 | RW | н | 16 | 12,1 | 90 | 4,6 | Sequen | | Ĺ |
| 89 | 2 | RW | H | 17 | 1,12 | 45 | 5,4 | Sequen | | Ĺ |
| 90 | 2 | RW | H | 15,18 | 11.1 | 45 | 1,6 | Sequen | | L |
| 91 | 2 | RW | F,H | 12,18 | 11,1 | Ø | 1,5 | Sequen | | L |
| 92 | 2 | RW | H,F | 18,12 | 11,1 | Ø | 2,6 | Sequen | | ML |
| 93 | 2 | RW | F,H | 11,17 | 12 | Ø | 4,3 | Sequen | 15 | ML |

| Scen | No. | | | Aircraf | t Clock | Degrees | Pattern | Pres. | Seconds | Diffic |
|----------|-----|------|---------|----------|----------|-----------|---------|--------|---------|----------|
| | | Type | Intent | Model | | | /Stand | Order | | Level |
| | | | | 16 14 | 12 | 45 | 4,3 | Sequen | 15 | L |
| 94 | 2 | RW | H,F | 16,14 | | 43 90 | 2,6 | Sequen | | L |
| 95 06 | 2 | RW | F,H | 13,15 | 11,1 | | 1,6 | Sequen | | L |
| 96 | 2 | RW | H,F | 12,16 | 11,1 | 0,45 Ø | 1,5 | Simult | | ML |
| 97 | 2 | RW | F | 11 | 11,1 | 9Ø | 2,6 | Simult | | ML |
| 98 | 2 | RW | F | 12,13 | 11,1 | | • | Simult | | ML |
| 99 | 2 | RW | F | 11,14 | 12 | 45 | 4,3 | Simult | | ML |
| 100 | 2 | RW | F | 12,13 | 11,12 | Ø,45 | 1,4 | | | |
| 101 | 2 | RW | H | 17 | 11,1 | Ø | 1,5 | Simult | | ML ML |
| 102 | 2 | RW | H | 18,17 | 11,1 | 90 | 2,6 | Simult | _ | |
| 103 | 2 | RW | H | 16,15 | 12 | 45 | 4,3 | Simult | | ML |
| 104 | 2 | RW | ä | 18,15 | 11,12 | 0,45 | 1,4 | Simult | | ML |
| 105 | 2 | RW | F,H | 12,18 | 11,1 | Ø | 1,5 | Simult | | ML |
| 106 | 2 | RW | F,H | 11,16 | 11,12 | 45 | 4,6 | Simult | | ML |
| 107 | 2 | RW | F,H | 13,17 | 11,1 | 45,0 | 2,5 | Simult | | ML |
| 108 | 2 | RW | F,H | 12,18 | 12 | 9Ø | 4,2 | Simult | | ML |
| 109 | 2 | RW | H,F | 15,14 | 1 | 45 | 6,5 | Simult | | ML |
| 110 | 2 | RW | H,F | 15,13 | 11,1 | 45 | 2,6 | Simult | | ML |
| 111 | 2 | RW | H,F | 17,11 | 11,12 | 0,45 | 1,4 | Simult | | ML |
| 112 | 2 | RW | H,F | 16,12 | 12,1 | 90,45 | 4,6 | Simult | | ML |
| 113 | 3 | RW | | 11,14,13 | 12,1,11 | 45 | 4,5,2 | Sequer | | ML |
| 114 | 3 | RW | | 13,14,12 | | 45 | 2,4,1 | Sequer | | ML |
| 115 | 3 | RW | | 18,15,17 | 12,11,1 | 45 | 4,2,5 | Seque | | ML |
| 116 | 3 | RW | | 16,18,17 | 1,12,1 | 45 | 6,4,5 | Sequer | 1 15 | ML |
| 117 | 3 | | | 13,16,12 | 11,1,12 | 45 | 2,5,3 | Sequer | | ML |
| 118 | 3 | RW | F,H,F | 11,18,12 | 11,12,1 | 90 | 1,4,6 | Sequer | | ML |
| 119 | 3 | | | 14,16,13 | 12,11,1 | Ø | 4,1,5 | Sequer | | М |
| 120 | 3 | | | 13,12,15 | | | 4,1,2 | Seque | | ML |
| 121 | 3 | RW | H,F,F | 16,11,11 | 12,1,1 | 45,45,0 | 4,6,5 | Sequer | | ML |
| 122 | 3 | | | 17,12,15 | 1,12,11 | 45 | 6,3,2 | Sequer | | ML |
| 123 | 3 | | | 18,11,17 | 11,12,1 | 90 | 2,4,5 | Sequer | | ML |
| 124 | 3 | RW | H,F,H | 18,14,15 | 1,12,11 | Ø | 5,4,2 | Sequer | | M |
| 125 | 3 | RW | F,H,H | 14,18,17 | 12,11,11 | 0,45,45 | 4,1,2 | Seque | | ML |
| 126 | 3 | RW | H,H,F | 16,17,13 | 12,1,1 | 45,45,0 | 4,6,5 | Seque | | ML |
| 127 | 3 | RW | F | 13,14,11 | 11,12,1 | 45 | 2,4,6 | Simult | | M |
| 128 | 3 | RW | | 12,14,13 | 11,12,1 | 45 | 1,3,5 | Simult | | M |
| 129 | 3 | RW | F | 12,11,12 | 11,12,1 | 0,90,45 | 1,4,6 | Simult | | M |
| 130 | 3 | RW | F | 14,11,13 | 11,1,1 | 90,45 | 2,5,6 | Simul | | M |
| 131 | 3 | RW | H | 15,16,17 | 11,12,1 | 45 | 2,4,6 | Simul | 60 | M |
| 132 | 3 | RW | H | 17,15,18 | 11,12,1 | 45 | 1,3,5 | Simul | 60 | M |
| 133 | 3 | RW | H | 16,18,16 | 11,12,1 | 0,90,45 | 1,4,6 | Simul | 60 | M |
| 134 | 3 | RW | Н | 18,17,16 | 11,1,1 | 90,45 | 2,5,6 | Simul | 60 | M |
| 135 | 3 | | | 11,17,11 | 11,12,1 | Ø | 1,3,5 | Simul | 60 | M |
| 136 | 3 | RW | | 12,16,13 | 1,12,11 | 45 | 6,4,2 | Simul | 60 | M |
| 137 | 3 | RW | | 14,15,13 | 12,1,11 | 90 | 4,6,2 | Simul | 60 | M |
| 138 | 3 | | | 14,13,17 | 11,12,1 | | 2,4,5 | Simul | | M |
| 139 | 3 | | | 12,11,15 | 11,12,1 | 0,45,0 | 1,4,6 | Simul | 60 | M |
| 140 | 3 | | | 15,12,13 | 11,12,1 | | 2,3,6 | Simul | 60 | M |
| 141 | 3 | | | 16,14,11 | 11,12,1 | | 1,3,6 | Simul | 60 | M |
| | - | •••• | , - , - | , , | ,,_ | | • . • . | | | |

| Scen | | Tuna | Inten | Aircraft | | | Pattern /Stand | Pres. | | |
|------|------|------|-------|-----------|-----------|---------|-------------------|--------|------|---|
| No. | rary | Type | Inten | c Model | AZ I MUCH | Aspect | / 3 cand | | | |
| 142 | 3 | RW | F,F,H | 11,13,15 | 11,1,11 | 45 | 1,5,2 | Simult | 60 | M |
| 143 | 3 | | | 17,14,12 | 1,12,1 | 45 | 5,4,6 | Simult | | M |
| 144 | 3 | RW | H,F,H | 17,12,17 | 11,12,1 | Ø | 1,3,5 | Simult | : 60 | М |
| 145 | 3 | RW | H,F,H | 16,11,15 | 1,12,11 | 45 | 6,4,2 | Simult | : 60 | M |
| 146 | 3 | RW | H,F,H | 16,11,15 | 12,1,11 | 90 | 4,6,2 | Simult | : 60 | М |
| 147 | 3 | RW | H,H,F | 18,16,12 | 11,12,1 | 0,90,45 | 2,4,5 | Simult | : 60 | M |
| 148 | 3 | | | 15,16,13 | 11,12,1 | 0,45,0 | 1,4,6 | Simult | : 60 | M |
| 149 | 3 | | | | 11,12,1 | 0,90,45 | 2,3,6 | Simult | | M |
| 150 | 3 | RW | F,H,H | 12,15,17 | 11,12,1 | 45,0,90 | 1,3,6 | Simult | : 60 | M |
| 151 | 3 | RW | H,H,F | 17,18,13 | 11,1,11 | 45 | 1,5,2 | Simult | 60 | M |
| 152 | 3 | RW | F,H,H | 11,18,16 | 1,12,1 | 45 | 5,4,6 | Simult | | M |
| 153 | 2 | MIX | F | 1,13 | 12 | 0,45 | C,4 | Simult | 40 | Н |
| 154 | 2 | MIX | F | 2,11 | 1,11 | 45 | D,1 | Simult | | H |
| 155 | 2 | XIM | F | 3,12 | 12,1 | 0,30 | C,6 | Simult | | Н |
| 156 | 2 | XIM | F | 2,14 | 10,1 | 90,45 | A,5 | Simult | | Ħ |
| 157 | 2 | MIX | F | 1,14 | 12 | Ø | C,3 | Simult | 40 | H |
| 158 | 2 | XIM | F | 3,11 | 1 | 45 | D,6 | Simult | | H |
| 159 | 2 | MIX | Н | 4,18 | 12 | 0,45 | C,4 | Simult | 40 | н |
| 160 | 2 | MIX | H | 5,17 | 11,1 | 45 | в,5 | Simult | 40 | H |
| 161 | 2 | MIX | Н | 6,15 | 12,1 | 0,90 | C,6 | Simult | 40 | Н |
| 162 | 2 | MIX | H | 5,16 | 2,11 | 90,45 | E,1 | Simult | 40 | н |
| 163 | 2 | XIM | н | 6,17 | 12 | Ø | C,3 | Simult | 40 | H |
| 164 | 2 | MIX | Н | 4,15 | 11 | 45 | B,2 | Simult | 40 | Н |
| 165 | 2 | MIX | F,H | 2,18 | 12 | Ø,45 | C,4 | Simult | | H |
| 166 | 2 | MIX | F,H | 3,16 | 11,1 | 45 | в,6 | Simult | | Н |
| 167 | 2 | XIM | F,H | 2,16 | 12,1 | 0,90 | C,6 | Simult | | Н |
| 168 | 2 | MIX | F,H | 1,17 | 2,11 | 90,45 | E,1 | Simult | | H |
| 169 | 2 | MIX | F,H | 3,15 | 12 | Ø | C,3 | Simult | | H |
| 170 | 2 | MIX | F,H | 1,15 | 11 | 45 | B,2 | Simult | | н |
| 171 | 2 | XIM | H,F | 5,11 | 12 | 0,45 | C.4 | Simult | 40 | H |
| 172 | 2 | MIX | H,F | 6,13 | 1,11 | 45 | D,2 | Simult | | H |
| 173 | 2 | MIX | H,F | 4,14 | 12,11 | 0,90 | C, 2 | Simult | | H |
| 174 | 2 | MIX | H,F | 4,11 | 10,1 | 90,45 | A,5 | Simult | | н |
| 175 | 2 | XIM | H,F | 5,12 | 12 | Ø | C,3 | Simul | | н |
| 176 | 2 | MIX | H,F | 6,12 | 1 | 45 | D,6 | Simult | | н |
| 177 | 3 | MIX | F | 1,12,11 | 12,11,1 | 0,45,45 | C,1,5 | Simul | | H |
| 178 | 3 | MIX | F | 2,14,14 | 12 | Ø | C,3,4 | Simul | | н |
| 179 | 3 | XIM | F | 3,11,13 | 1,1,11 | 45 | D,6,2 | Simul | | н |
| 180 | 3 | MIX | F | 2,14,12 | 10,12,1 | | A,3,6 | Simul | | н |
| 181 | 3 | MIX | H | 4,16,18 | 12,11,1 | | C,1,5 | Simul | | H |
| 182 | 3 | MIX | Н | 6,17,17 | 12 | 0 | C,3,4 | Simul | | H |
| 183 | 3 | XIM | Н | 5,15,16 | 11,11,1 | 45 | В,2,6 | Simul | | H |
| 184 | 3 | XIM | H | 4,16,15 | 10,1,12 | • | A,6,3 | Simul | | H |
| 185 | 3 | | F,F,H | 1,14,16 | 12,11,1 | | C,2,6 | Simul | | H |
| 186 | 3 | | F,F,H | 2,12,18 | 11,11,1 | 45,0,0 | B,1,5 | Simul | | H |
| 187 | 3 | | F,H,F | 3,17,13 | 12 | ø | C,3,4 | Simul | | H |
| 188 | 3 | XIM | F,H,F | 1,15,11 | 1,12,1 | 45 | D,2,6 | Simul | t 60 | H |

| Scen No. | | | Intent | | ft Clock Azimut | | I | | Seconds Avail. | |
|-------------|---|-----|--------|---------|---------------------|----------|-------|--------|-------------------|---|
| 189 | 3 | MIX | F,H,H | 2,16,18 | 2,1,12 | 90,45,0 | E,6,4 | Simult | : 60 | H |
| 190 | 3 | MIX | F,H,H | 3,17,17 | 12,11,1 | 45,45,0 | C,1,5 | Simult | : 60 | H |
| 191 | 3 | MIX | F,H,H | 2,18,15 | 10,11,12 | 90,45,45 | A,2,3 | Simult | 60 | H |
| 192 | 3 | MIX | H,H,F | 4,15,12 | 12,11,1 | 0,45,45 | C,2,6 | Simult | : 60 | H |
| 193 | 3 | MIX | H,H,F | 5,16,11 | 11,11,1 | 45,0,0 | B,1,5 | Simult | : 60 | н |
| 194 | 3 | MIX | H,H,F | 5,15,11 | 11,11,1 | 45,0,0 | B,2,6 | Simult | : 60 | H |
| 195 | 3 | XIM | H,F,H | 6,14,18 | 12 | Ø | C,3,4 | Simult | 60 | H |
| 196 | 3 | XIM | H,F,H | 4,13,17 | 1,12,1 | 45 | D,2,6 | Simult | : 6Ø | H |
| 197 | 3 | XIM | H,F,H | 6,14,17 | 1,11,12 | 45,90,90 | D,2,6 | Simult | : 6Ø | H |
| 198 | 3 | MIX | H,F,F | 5,13,12 | 2,1,12 | 90,45,0 | E,6,4 | Simult | : 60 | H |
| 199 | 3 | MIX | H,F,F | 6,11,11 | 12,11,1 | 45,45,0 | C,1,5 | Simult | 60 | H |
| 200 | 3 | XIM | H,F,F | 4,14,12 | 10,11,12 | 90,45,45 | A,2,3 | Simult | : 60 | н |

AIRCRAFT MODEL TYPES

| FRIENDLY | HOSTILE |
|----------|----------------|
| FW: | FW: |
| 1=A7 | 4=MiG27 |
| 2=A1Ø | 5=Sul7 |
| 3=F16 | 6=Su25 |
| RW: | RW: |
| 11=AH64 | 15=Mi8 |
| 12=UH1 | 16=Mi24 |
| 13=UH6Ø | 17=Mi28 |
| 14=CH3 | 18=Mi? (Hokum) |

FW AIRCRAFT PATTERNS

| A | 9Ø | degree | crossing | pattern | commencing | at | 10:00 | azimuth |
|---|--------|--------|----------|---------|------------|----|-------|---------|
| | | | | | | | | |

$${\tt C}$$
 -- ${\tt Ø}$ degree ingress pattern commencing at 12:00 azimuth

RW AIRCRAFT STANDS

| 1 | 3 | kilometer | target | at | 11:00 | azimuth |
|---|---|-----------|--------|----|-------|---------|
|---|---|-----------|--------|----|-------|---------|

6 -- 5 kilometer target at 1:00 azimuth

| 2 | 4 | 6 | • 5 | km |
|-------|-------|------|--------|----|
| 1 | 3 | 5 | 3 | km |
| 11:00 | 12:00 | 1:00 | | |

E -- 90 degree crossing pattern commencing at 2:00 azimuth

SCENARIO DIFFICULTY RATINGS

- o Extra High Difficulty (XH). Refers to scenarios having 2 or more targets flying tactical maneuvers.
- o High Difficulty (H). FW aircraft, due to their speed, maneuverability, range, and altitude present a more difficult adversary than their RW counterparts, especially when they ingress at zero aspect. A FW target presented simultaneously with multiple RW threats further taxes the soldiers' abilities. Mixed (FW and RW) scenarios thus represent a high degree of difficulty. Scenarios presenting multiple FW threats would likely be one or two levels of difficulty higher than this (XH).
- o Medium High Difficulty (MH). Based on the definition of high difficulty given above, the next difficulty level reflects single FW targets presented at Ø to 45 degrees aspect.
- o Medium Difficulty (M). This level reflects single, crossing FW scenarios at 90 degrees aspect. Also included are triple-simultaneous RW scenarios. The multiple RW threat makes for a challenging scenario in terms of soldier workload.
- o Medium Low Difficulty (ML). This level represents the doublesimultaneous RW scenario, and single or double-sequential RW scenarios presenting targets at maximum ranges or with small profiles (zero aspect). Moderate workload or moderate target visibility help to distinguish this from the lowest difficulty level.
- o Low Difficulty (L). RW targets that are close in range or present a side view orientation are easy to detect and identify, and are rapidly engaged. Therefore, single, or double-sequential RW scenarios appear to be the easiest ones.

APPENDIX B

PROCEDURES FOR ASSESSING SCENARIO DIFFICULTY

Scenario Difficulty Weighting Procedure

- 1. A list was generated consisting of 14 difficulty factors having subfactors within each factor.
- Five Subject Matter Experts (SME) weighted each factor for difficulty on a scale of from 1 to 100 (l=easiest, 100=hardest). The sum of the 14 factor weights always equaled 100.
- 3. Each of the 14 factors contained subfactors (e.g., Model Type factor contained a subfactor for each aircraft model being used). Each SME rated each subfactor for difficulty on a scale of 1 to 100 (subfactor values did not have to sum to 100).
- 4. 20 scenarios were developed. Each scenario was weighted using the factor and subfactor scores from each SME. Scenario difficulty scores represented subfactor weights multiplied by associated factor weights and summed over all 14 factors. Thus, a point total existed for each of the 20 scenarios for each SME.
- 5. For each SME, raw scenario scores were transformed to standard scores of 1 to 5 (1=1ow, 2=medium-low, 3=medium, 4=medium-high, 5=high) using the following procedure:
 - a. Scenario scores were transformed into proportion scores by dividing each weight by the largest weighting score given by that specific SME. (Example: If an SME rated 3 scenarios 50, 55, 65, then each scenario would be turned into a proportion score with 65 as the denominator. 50/65=.77, 55/65=.85, 65/65=1.00.) Thus, each weighting score was turned into a proportion score with each base being that SME's highest rating, thereby controlling for differences between raters in highest score given and range of scores.
 - b. Proportion scores ranged from lowest to 1.00 across all the 20 scenarios. This total range for each SME was divided into 5 equal-sized categories. (In the example above: Range was 1.00 minus 0.77=0.23. This .23 range was divided into 5 parts; .770-.816, .816-.862, .862-.908, .908-.954, .954-1.00.) These 5 equal-sized categories were given the numbers 1 to 5. (Lowest category=1, highest category=5)

6. SME's ratings (now labelled 1-5) were then summed and averaged for each of the 20 scenarios. That is, the mean SME rating was determined for each scenario. Each scenario was given a final label of L, ML, M, MH, or H which corresponded to the mean SME rating. This is how the SME weightings became difficulty indices for each of the 20 scenarios.

Factors

- Criterion 1: Target Type (FW or RW) -- RW targets are generally easier to detect and identify than FW targets because they are usually closer in range upon initial line-of-sight, and do not roll, pitch, or yaw.
- Criterion 2: Target Size -- Target model types vary from small (UH1) to large (MI8). The larger models are easier to see, and therefore to detect and identify.
- Criterion 3: Target Model -- Soldiers are typically more familiar with some aircraft model types than others. For example, soldiers are better at identifying the Hind-D than the Havoc.
- Criterion 4: Target Range -- Obviously, the farther away the target appears, the harder it is to detect and identify. This variable is especially relevant for RW targets as they do not vary in range once exposed. Thus, the farther away they are presented, the higher the LOD should be. For FW, the target will almost always begin its approach from beyond visible range when ingressing.
- Criterion 5: Target Aspect and Offset -- Targets with side view orientations are easier to detect and to identify than face view (i.e., head-on) orientations because the target subtends a larger visual angle, and because more target features are visible. Further, the farther the target is from the fire unit's primary target line or from a cued azimuth, the longer it will take to detect it.
- Criterion 6: Target Altitude -- Aircraft flying nap-of-the-earth or at extremely high altitudes are more difficult to see than those flying at moderate altitudes. Further, low targets are easier to see as the elevation above the terrain mask increases.
- Criterion 7: Target Speed and Maneuverability -- Aircraft flying extremely fast will be harder to see and will present themselves for a shorter period of time than those flying at slower speeds. Further, maneuvering (dynamic) targets will be harder to detect and engage than static ones.

- Criterion 8: Target Intent (Friendly or Hostile) -- RADES research has demonstrated that air defenders are typically faster and more accurate in responding to hostile targets than friendly targets. They tend to adopt "hostile expectancies" whereby the target default is hostile when there is doubt about its intent.
- Criterion 9: Visibility and Contrast Conditions -- While the typical simulation environment will have clear weather, daylight, sky background, and non-obscured viewing conditions, this will not always be the case in real life situations. In order to generalize a scenario to other viewing situations, there must be some metric to gauge the extent to which reduced visibility will increase difficulty level. Visibility can be affected by atmospheric conditions (e.g. rain, etc.), windspeed, cloudiness, battlefield obscurants, etc.
- Criterion 10: Terrain Conditions -- While the typical simulation environment will be the desert environment with a sky target background, such is not always the case in the real world. Greater difficulty would be expected for environments 'aving more dense terrain, terrain target occulting (obscuration), or a lower contrast ratio between target and background.
- Criterion 11: Weather Conditions -- It is well known that performance will drop as a result of extreme temperatures or weather conditions. This criterion relates only to the effect of weather on the soldier's physical abilities, and not on visibility which was covered previously.
- Criterion 12: Number of Targets -- More than one target can improve detection time since there is a greater likelihood that a target will appear in the observer's field-of-view. However, multiple targets may also create confusion or panic in the other engagement tasks since it becomes more difficult to sort out the friends from the foes, and engage the target posing the greatest threat. Therefore, multiple target scenarios are usually associated with greater difficulty.
- Criterion 13: Saturation Level -- This criterion relates primarily to workload level as influenced by battlefield situations. The more fatigued, tired, or inattentive the soldier is, the poorer his performance will be. A fire unit that has reacted to 30 scenarios will likely be more tired than one that has only responded to 3 scenarios during the same time frame; but the level of expectancy for that fire unit will likely be greater as well, while the latter fire unit may be less attentive. Generally, higher saturation level is equated to greater difficulty.

Criterion 14: C3I Conditions -- The use of doctrine, tactics, and C3I vary from one scenario to another and can cause drastic effects on performance, especially if the relevant information is not easily interpretable or if it is untimely or inaccurate. Combinations of message traffic or alerting and cuing updates can be consistent or conflicting; the more conflicting the inputs, the more confusion that ensues, resulting in either hesitation or panic on the part of the fire unit. For example, inputs such as WCS free, air defense warning red, and IFF return unknown are all consistent in suggesting that an approaching aircraft is hostile. This would substantially lower the difficulty level.

Subfactors

Criterion 1: Target Type FW, RW, or Mixed

Criterion 2: Target Size Small (UHl or A7) Medium (AH64 or Al0) Large (MI24 or SU17) Extra Large (MI8 or SU24)

Criterion 3: Target Model

A7 (Corsair), AlØ (Thunderbolt), Fl6 (Fighting Falcon), F111, SU7 (Fitter), SU17/20/22 (Fitter), SU24 (Fencer), SU25 (Frogfoot), MIG27 (Flogger)

UHl (Iroquois), UH60 (Blackhawk), AHl (Cobra), AH64 (Apache), CH3 (Green Giant), MI8 (Hip), MI24 (Hind), MI28 (Havoc), MI? (Hokum)

Criterion 4: Target Range 1-2 km, 3-4 km, 5-6 km, 7-8 km, 9-10 km, 11-14 km, 15-20 km

Criterion 5: target Aspect

90 degrees (side view) 60 degrees (side-tail view)

60 degrees (side-face view)

30 degrees (side-tail view)

30 degrees (side-face view)

Ø degrees (tail view)

0 degrees (face view)

Criterion 6: Target Altitude

0 - 1 degrees above horizon

1.5 - 3 degrees above horizon

3.5 - 5 degrees above horizon

6 - 10 degrees above horizon

11 - 15 degrees above horizon

16 - 25 degrees above horizon

```
Criterion 7: Target Speed (based on 1/7 scale aircraft)
         0 - 10 Mph (RW hover)
        40 - 70 Mph (RW maneuver)
       90 - 120 Mph (FW maneuver)
      120 - 180 Mph (FW flyby)
Criterion 8: Target Intent
      Friendly or Hostile
Criterion 9: Visibility and Contrast Conditions
      1-2 \text{ km}, 3-5 \text{ km}, 6-10 \text{ km}, 11-20 \text{ km}, 21-40 \text{ km}, 41+ \text{ km}
      Clear Sky, Partly Cloudy, Overcast
Criterion 10: Terrain Conditions
      Desert, Forest, Jungle
      Sky Background, Terrain Background
Criterion 11: Weather Conditions
      -10 to 20 degrees F
        21 -- 40 degrees F
       41 -- 60 degrees F
       61 -- 80 degrees F
       31 -- 100 degrees F
            101+ degrees F
Criterion 12: Number of Targets
      1, 2, 3, 4, or 5
Criterion 13: Saturation Level
    Scenarios per day:
      1 - 2 Scenarios per day
3 - 9 Scenarios per day
10 - 24 Scenarios per day
       25 - 40 Scenarios per day
            41+ Scenarios per day
    Arousal Level:
        Fresh, Average, Fatigued
Criterion 14: C<sup>3</sup>I Conditions
    Alert, WCS, IFF:
      Red, Free
      Red, Tight
      Red, Free, & IFF Unknown
      Red, Free, & IFF Possible Friend
      Red, Tight, & IFF Unknown
      Red, Tight, & IFF True Friend
    Alerting and Cuing
       Alert Once per Day
      Alert Once per Trial
      Alert & Cue (+ / -15 degrees accuracy)
Alert & Cue (+ / -5 degrees accuracy)
```

APPENDIX C DESCRIPTIVE STATISTICS ON 20 STANDAPL SCENARIOS

SCENARIO 2 DESCRIPTIVES

ORD

1.00 0.00 7

Table Cl Scenario Descriptive Statistics (Range=kilometers; Time=seconds; Proportion=percent; N=number of teams)

SCENARIO 1 DESCRIPTIVES

| TARGET | VARIABLE | MEAN | SD | N | TARGET | VARIABLE | MEAN | SD | N |
|----------|--|--|---|---------------------------------|---------|--|--------------|---|---|
| 1(A1Ø) | RDET RIFF RID TID RACQ IDCOR FIRED FRAT | 10.0 7.3 17.7 7.5 0.83 0.00 0.00 | 3.3 3.7 2.5 8.4 Ø.0 Ø.41 Ø.00 | 6 4 6 6 1 6 6 | 1 (F16) | RIFF RID TID RACQ RLOCK RFIRE TTOT IDCOR FIRED EFFECT FRAT | Ø.00 Ø.00 | 2.0 2.5 2.5 4.5 0.9 0.8 0.5 16.3 0.55 0.00 | 6 |
| SCENARIO | O 3 DESCRI | PTIVES | | | SCENARI | O 4 DESCRI | PTIVES | | |
| TARGET | VARIABLE | MEAN | SD | N | TARGET | VARIABLE | MEAN | SD | N |
| 1(F111) | RDET RIFF | 7.6 | Ø.7 | 7 | 1(MIG27 |)RDET | 10.7 | 2.8 | |

Table Cl (Continued) Scenario Descriptives

SCENARIO 5 DESCRIPTIVES SCENARIO 6 DESCRIPTIVES

| TARGET | VARIABLE | MEAN | SD | N | TARGET | VARIABLE | MEAN | SD | N |
|---------|----------|------|------|---|---------|----------|------|------|---|
| 1(SU25) | RDET | 11.6 | 2.9 | 3 | 1(SU24) | RDET | 7.8 | 0.7 | 7 |
| | RIFF | 8.7 | Ø.3 | 3 | | RIFF | 7.3 | Ø.5 | 7 |
| | RID | 7.2 | 0.8 | 2 | | RID | 5.8 | 0.3 | 7 |
| | TID | 18.0 | 8.5 | 2 | | TID | 13.6 | 3.3 | 7 |
| | RACQ | 5.5 | 1.2 | 3 | | RACQ | 6.2 | 0.4 | 7 |
| | RLOCK | 5.2 | 0.0 | 1 | | RLOCK | 5.8 | 0.4 | 7 |
| | RFIRE | 4.8 | Ø.1 | 2 | | RFIRE | 5.9 | 0.6 | 7 |
| | TOTT | 28.0 | 11.3 | 2 | | TTOT | 19.7 | 3.3 | 7 |
| | IDCOR | Ø.67 | 0.58 | 3 | | IDCOR | Ø.67 | Ø.58 | 3 |
| | FIRED | Ø.67 | 0.58 | 3 | | FIRED | 1.00 | 0.00 | 7 |
| | EFFECT | Ø.5Ø | 0.71 | 2 | | EFFECT | Ø.57 | 0.53 | 7 |
| | ATTRIT | Ø.33 | | 3 | | ATTRIT | Ø.57 | | 7 |
| | ORD | 1.00 | | 3 | | ORD | 0.00 | 0.00 | 7 |
| | | | | | | | | | |

SCENARIO 7 DESCRIPTIVES SCENARIO 8 DESCRIPTIVES

| TARGET | VARIABLE | MEAN | SD | N | TARGET | VARIABLE | MEAN | SD | N |
|---------|---|--|---|---|--------|---|--|--|--|
| 1(UH60) | TDET TIFF TID TACQ TLOCK TFIRE TTOT IDCOR FIRED EFFECT FRAT | 3.4 3.0 8.7 5.3 2.7 3.0 10.0 0.57 0.14 1.00 0.14 | 1.1 2.8 4.2 1.6 0.6 0.0 0.0 0.53 0.38 0.00 | 7 7 7 6 3 1 1 7 7 | 1(CH3) | TDET TIFF TID TACQ TLOCK TFIRE TTOT THAND IDCOR FIRED EFFECT FRAT | 2.7 5.8 4.1 3.7 2.7 3.0 9.0 5.3 0.29 0.43 0.67 0.29 | 2.0 6.8 2.0 1.9 1.2 0.0 1.0 1.5 0.49 0.53 0.58 | 7 5 7 4 3 2 3 7 7 3 |

Table Cl (Continued) Scenario Descriptives

SCENARIO 9 DESCRIPTIVES SCENARIO 10 DESCRIPTIVES

| TARGET | VARIABLE | MEAN | SD | N | TARGET | VARIABLE | MEAN | SD | N |
|--------|-----------------|------|------|---|--------|----------|------|------|--------|
| 1(MI?) | TDET | 4.5 | 3.6 | 8 | 1(MI8) | TDET | 5.5 | 6.8 | 8 |
| | TIFF | 1.5 | 1.0 | 7 | | TIFF | 1.7 | 1.1 | 7 |
| | TID | 5.7 | 3.0 | 8 | | TID | 5.2 | 3.Ø | 8 |
| | \mathtt{TACQ} | 5.Ø | 2.2 | 7 | | TACQ | 4.9 | 2.0 | 8 |
| | TLOCK | 2.6 | 1.0 | 7 | | TLOCK | 2.0 | Ø.6 | 7 |
| | TFIRE | 3.6 | 3.4 | 7 | | TFIRE | 2.3 | Ø.8 | 6 |
| | TTOT | 11.1 | 4.3 | 7 | | TTOT | 9.1 | 2.9 | 6 |
| | THAND | 6.5 | 4.8 | 6 | | THAND | 4.6 | 1.8 | 5 |
| | IDCOR | Ø.87 | Ø.35 | 8 | | IDCOR | Ø.87 | Ø.35 | 8 |
| | FIRED | | Ø.35 | 8 | | FIRED | Ø.75 | 0.46 | 8 |
| | EFFECT | | Ø.38 | 7 | | EFFECT | Ø.67 | Ø.51 | 6 |
| | FRAT | Ø.75 | | 8 | | FRAT | 0.50 | | 8 |
| | ORD | Ø.62 | Ø.52 | 8 | 2(MI8) | TDET | 22.7 | 1.2 | 6 |
| | | | | | | TIFF | 2.2 | 1.9 | 5 |
| | | | | | | TID | 4.7 | 1.9 | 6 |
| | | | | | | TACQ | 5.4 | 2.1 | 3 3 |
| | | | | | | TLOCK | 2.3 | 2.1 | 3 |
| | | | | | | TFIRE | 2.0 | 0.0 | 3 |
| | | | | | | TTOT | 9.7 | 2.2 | 4 |
| | | | | | | THAND | 4.7 | 1.5 | 4 |
| | | | | | | IDCOR | Ø.75 | 0.46 | 8 |
| | | | | | | FIRED | 0.50 | 0.53 | 8 |
| | | | | | | EFFECT | 0.25 | Ø.5Ø | 4 |
| | | | | | | ATTRIT | Ø.12 | | 8 |
| | | | | | | ORD | Ø.87 | Ø.35 | 8 |

Table Cl (Continued) Scenario Descriptives

SCENARIO 11 DESCRIPTIVES SCENARIO 12 DESCRIPTIVES

| | | | | | | | | |
|---------|----------|---------------|------|---|--------|-----------------|---|---------------------------------------|
| TARGET | VARIABLE | MEAN | SD | N | TARGET | TARGET VARIABLE | TARGET VARIABLE MEAN | TARGET VARIABLE MEAN SD |
| 1(MI24) | TDET | 3.6 | 1.4 | 7 | 1(AH1) | l(AHl) TDET | 1(AH1) TDET 4.0 | 1(AH1) TDET 4.0 1.9 |
| · | TIFF | 8.9 | 6.9 | 7 | | TIFF | | |
| | TID | 5.0 | 1.8 | 6 | | TID | TID 6.2 | TID 6.2 2.8 |
| | TACQ | 4.6 | 3.Ø | 5 | | TACQ | TACQ 5.6 | TACQ 5.6 1.7 |
| | TLOCK | 3.0 | 1.0 | 4 | | TLOCK | TLOCK 5.0 | TLOCK 5.0 2.8 |
| | TFIRE | 2.3 | 0.6 | 3 | | TFIRE | TFIRE 2.0 | TFIRE 2.0 0.0 |
| | TTOT | 9.0 | 2.0 | 3 | | TTOT | TTOT 11.0 | TTOT 11.0 0.0 |
| | THAND | 3.7 | 3.2 | 3 | | THAND | THAND 7.0 | THAND 7.0 0.0 |
| | IDCOR | Ø . 57 | Ø.53 | 7 | | IDCOR | IDCOR 0.87 | IDCOR 0.87 0.35 |
| | FIRED | 0.43 | Ø.53 | 7 | | FIRED | FIRED 0.12 | FIRED 0.12 0.35 |
| | EFFECT | 1.00 | 0.00 | 3 | | EFFECT | EFFECT 1.00 | EFFECT 1.00 0.00 |
| | ATTRIT | 3.43 | | 7 | | FRAT | | |
| 2(MI24) | TDET | 25.2 | 3.3 | 5 | 2(UH1) | 2(UH1) TDET | | · |
| | TIFF | 2.7 | 2.9 | 4 | | TIFF | · - | |
| | TID | 2.2 | 1.3 | 5 | | TID | - | |
| | TACQ | 3.4 | 2.1 | 5 | | TACQ | ~ | |
| | TLOCK | 2.Ø | Ø.8 | 4 | | TLOCK | | |
| | TFIRE | 1.7 | 1.0 | 4 | | TFIRE | - · · · · · · · · · · · · · · · · · · · | |
| | TTOT | 6.4 | 3.6 | 5 | | TTOT | | · · · · · · · · · · · · · · · · · · · |
| | THAND | 4.2 | 2.4 | 5 | | THAND | · · · · · · · · · · · · · · · · · · · | |
| | IDCOR | Ø.71 | 0.49 | 7 | | IDCOR | | |
| | FIRED | Ø.71 | - • | 7 | | FIRED | | |
| | EFFECT | | 0.00 | 5 | | EFFECT | | |
| | ATTRIT | Ø.Ø | | 7 | | FRAT | FRAT Ø.25 | FRAT Ø.25 |
| | ORD | Ø.86 | 0.38 | 7 | | | | |

Table Cl (Continued) Scenario Descriptives

SCENARIO 13 DESCRIPTIVES SCENARIO 14 DESCRIPTIVES

| SCENARI | O 13 DE3CR | 161145 | | | SCENARI | O 14 DESCR | 1511163 |) . | |
|---------|------------|--------|---------------|---|----------|------------------|--------------|--------------------|--------|
| TARGET | VARIABLE | MEAN | SD | N | TARGET | VARIABLE | MEAN | SD | N |
| 1(MIS) | TDET | 5.7 | 3.4 | 8 | 1(CH3 | TDET | 2.5 | 1.0 | 7 |
| | TIFF | 9.3 | 8.5 | 7 | or | TIFF | 3.9 | 4.7 | 7 |
| | TID | 6.6 | 2.9 | 8 | MI8) | TID | 6.0 | 1.6 | 7 |
| | TACQ | 5.5 | 4.4 | 8 | | TACQ | 5.7 | 1.5 | 6 |
| | TLOCK | 6.1 | 9.7 | 8 | | TLOCK | 3.2 | 2.5 | 6 |
| | TFIRE | 2.4 | 1.3 | 7 | | TFIRE | 2.3 | 1.5 | 6 |
| | TTOT | 11.4 | 3.4 | 7 | | TTOT | 11.2 | 2.7 | 6 |
| | THAND | 5.0 | 3.3 | 7 | | THAND | 5.0 | 1.8 | 6 |
| | IDCOR | | 0.35 | 8 | | IDCOR | 0.14 | 0.38 | 7 |
| | FIRED | Ø.87 | Ø.35 | 8 | | FIRED | Ø.86 | Ø.38 | 7 |
| | EFFECT | | Ø.53 | 7 | | EFFECT | 1.00 | 0.00 | 6 |
| | ATTRIT | | | 8 | 2 (CH 3 | TDET | 20.4 | 7.5 | 7 |
| | ORD | 1.00 | | 8 | or | TIFF | 3.6 | 5.5 | 7 |
| 2(MI24) | | 33.5 | 3.0 | 6 | MI8) | TID | 4.9 | 2.3 | 7 |
| | TIFF | Ø.8 | 1.0 | 6 | | TACQ | 7.4 | 6.0 | 7 |
| | TID | 8.0 | 3.2 | 6 | | TLOCK | 3.9 | 2.3 | 7 |
| | TACQ | 6.0 | 5.2 | 5 | | TFIRE | 1.7 | Ø.5 | 7 |
| | TLOCK | 2.2 | Ø.5 | 4 | | TTOT | 13.0 | 5.4 | 7 |
| | TFIRE | 3.2 | 2.2 | 4 | | THAND | 8.1 | 5.8 | 7 |
| | TTOT | 12.5 | 5.5 | 4 | | IDCOR | 1.00 | 0.00 | 7 |
| | THAND | 5.Ø | 4.5 | 4 | | FIRED | 1.00 | | 7 |
| | IDCOR | | 0.52 | 8 | 2 | EFFECT | Ø.71 | | 7 |
| | FIRED | | 0.53 | 8 | CH3 | IDCOR | 0.14 | | 7 |
| | EFFECT | | Ø . 57 | 4 | | FIRED | Ø.86 | 0.38 | 7 |
| | ATTRIT | Ø.25 | | 8 | | EFFECT | 1.00 | - | 6 |
| | ORD | שש. ב | 0.00 | 8 | M T O | FRAT | 0.86 | 0.38 | 7 |
| | | | | | MI8 | IDCOR | 1.00 | 0.00 | 7 |
| | | | | | | FIRED | 1.00 0.71 | _ | 7 7 |
| | | | | | | EFFECT ATTRIT | Ø.71 | | 7 |
| | | | | | | ORD | 1.00 | | 7 |
| | | | | | | OKD | 1.00 | שש.ש | , |

Table Cl (Continued) Scenario Descriptives

SCENARIO 15 DESCRIPTIVES SCENARIO 16 DESCRIPTIVES

| TITLE TO BE CALLET TO BE CALLED | | | | | OCDIVATIO TO DEDCKITITIO | | | | | |
|--|----------|------|------|---|--------------------------|----------|------|------|---|--|
| TARGET | VARIABLE | MEAN | SD | N | TARGET | VARIABLE | MEAN | SD | N | |
| 1(MI8 | TDET | 3.1 | 1.3 | 7 | 1(AH1 | TDET | 8.9 | 12.9 | 7 | |
| or | TIFF | 3.6 | 5.1 | 5 | or | TIFF | 3.5 | 4.4 | 6 | |
| MI28 | TID | 4.7 | 1.9 | 7 | MI 28 | TID | 5.3 | 3.7 | 6 | |
| or | TACQ | 3.9 | 2.5 | 7 | or | TACQ | 7.3 | 2.1 | 3 | |
| MI24) | TLOCK | 3.2 | 1.5 | 6 | MI24) | TLOCK | 3.8 | 1.1 | 5 | |
| | TFIRE | 2.2 | Ø.5 | 5 | | TFIRE | 4.2 | 6.0 | 4 | |
| | TTOT | 8.8 | 1.3 | 6 | | TTOT | 8.7 | 5.2 | 4 | |
| | THAND | 4.3 | Ø.8 | 6 | | THAND | 6.0 | 6.4 | 5 | |
| | IDCOR | Ø.86 | Ø.38 | 7 | | IDCOR | Ø.71 | 0.49 | 7 | |
| | FIRED | Ø.71 | 0.49 | 7 | | FIRED | Ø.71 | 0.49 | 7 | |
| | EFFECT | 0.80 | 0.45 | 5 | | EFFECT | Ø.6Ø | 0.54 | 5 | |
| 2(MI8 | TDET | 17.6 | 2.0 | 7 | 2(AH1 | TDET | 18.6 | 7.5 | 5 | |
| or | TIFF | Ø.8 | 1.0 | 6 | or | TIFF | 4.0 | 4.1 | 5 | |
| MI28 | TID | 4.2 | 1.2 | 6 | MI28 | TID | 6.4 | 2.2 | 5 | |
| or | TACQ | 4.7 | 1.5 | 6 | or | TACQ | 3.2 | 2.2 | 5 | |
| MI24) | TLOCK | 2.5 | 1.4 | 6 | MI24) | TLOCK | 5.3 | 3.1 | 3 | |
| | TFIRE | 2.2 | Ø.8 | 6 | | TFIRE | 2.0 | 1.0 | 3 | |
| | TTOT | 9.3 | 1.4 | 6 | | TTOT | 8.7 | 3.8 | 4 | |
| | THAND | 5.2 | Ø.8 | 6 | | THAND | 2.7 | 3.2 | 4 | |
| | IDCOR | | Ø.38 | 7 | | IDCOR | Ø.57 | Ø.53 | 7 | |
| | FIRED | | Ø.38 | 7 | | FIRED | Ø.57 | | 7 | |
| | EFFECT | | 0.00 | 6 | | EFFECT | 0.50 | | 4 | |
| 3(MI8 | TDET | 30.7 | 4.0 | 7 | 3(AH1 | TDET | 31.8 | 8.3 | 5 | |
| or | TIFF | 3.0 | 2.8 | 7 | or | TIFF | 1.0 | 1.0 | 3 | |
| MI28 | TID | | 3.8 | 7 | MI28 | TID | 6.5 | 1.3 | 4 | |
| or | TACQ | | 4.2 | 6 | or | TACQ | 4.0 | 2.7 | 4 | |
| MI24) | _ | | 1.9 | 5 | MI24) | | 4.0 | 0.0 | 1 | |
| • | TFIRE | 1.8 | 0.4 | 5 | , | TFIRE | 2.0 | 0.0 | 1 | |
| | TTOT | | 4.9 | 5 | | TTOT | 17.7 | 10.0 | 3 | |
| | THAND | 4.0 | 1.9 | 5 | | THAND | 11.7 | 10.8 | 3 | |
| | IDCOR | | Ø.38 | 7 | | IDCOR | 0.43 | 0.53 | | |
| | FIRED | | 0.49 | 7 | | FIRED | Ø.57 | 0.53 | 7 | |
| | EFFECT | | Ø.55 | 5 | | EFFECT | 0.00 | 0.00 | 3 | |
| MI8 | IDCOR | | 0.00 | 7 | AHl | IDCOR | 0.57 | | 7 | |
| | FIRED | | 0.00 | 7 | | FIRED | Ø.57 | 0.53 | | |
| | EFFECT | Ø.86 | 0.38 | 7 | | EFFECT | 0.25 | 0.50 | | |
| | ATTRIT | Ø.86 | | 7 | | FRAT | Ø.14 | | 7 | |
| | ORD | | 0.00 | 7 | MI24 | IDCOR | 0.57 | 0.53 | 7 | |
| MI28 | IDCOR | | 0.49 | 7 | | FIRED | Ø.71 | 0.49 | | |
| | FIRED | | 0.49 | 7 | | EFFECT | Ø.6Ø | Ø.55 | | |
| | EFFECT | | 0.00 | 5 | | ATTRIT | 0.43 | | 7 | |
| | ATTRIT | | | 7 | | ORD | 1.00 | 0.00 | 7 | |
| | ORD | | 0.00 | 7 | MI28 | IDCOR | Ø.57 | Ø.53 | | |
| MI24 | IDCOR | | 0.38 | 7 | | FIRED | 0.43 | 0.53 | | |
| | FIRED | | 0.53 | 7 | | EFFECT | 0.33 | Ø.58 | | |
| | EFFECT | | 0.50 | 4 | | ATTRIT | 0.14 | | 7 | |
| | ATTRIT | | | 7 | | ORD | 1.00 | 0.00 | 7 | |
| | ORD | | 0.00 | 7 | | | | | | |

Table Cl (Continued) Scenario Descriptives

| TARGET | VARIABLE | MEAN | SD | N |
|----------|-----------------|--------------|--------------|-----------------------|
| 1(CH3 | TDET | 1.3 | Ø . 5 | 7 |
| or | TIFF | 2.3 | 2.4 | 7 |
| MI28 | TID | 4.0 | 1.8 | 7 |
| or | TACQ | 4.4 | 1.3 | 5 |
| UH1) | TLOCK | 2.2 | 1.6 | 5 |
| | TFIRE | 1.8 | Ø.8 | 5 |
| | TTOT | 8.4 | 1.8 | 5 |
| | THAND | 4.6 | 2.3 | 5 |
| | IDCOR | Ø.81 | Ø.49 | 7 |
| | FIRED | Ø.71 | 0.49 | 7 |
| | EFFECT | 1.00 | 0.00 | 5 |
| 2 (CH 3 | TDET | 13.1 | 1.8 | 7 |
| or | TIFF | 2.4 | 2.9 | 7 |
| MI28 | TID | 4.1 | 2.9 | 7 |
| or | TACQ | 3.2 | 2.2 | 4 |
| UHl) | TLOCK | 2.0 | 1.4 | 2 |
| | TFIRE | 2.0 | 0.0 | 3 |
| | TTOT | 7.7 | 1.5 | 3 |
| | THAND | 5.0 | 0.0 | 3 |
| | IDCOR | Ø.57 | | 7 |
| | FIRED | 0.43 | Ø.53 | 7 |
| * 4 = | EFFECT | Ø.67 | 0.58 | 3 |
| 3 (CH3 | TDET | 25.3 | 4.9 | 7 |
| or | TIFF | 3.5 | 6.7 | 6 |
| MI28 | TID | 7.3 | 5.3 | 7 |
| or | TACQ | 5.5 | 1.3 | 4 |
| UH1) | TLOCK | 3.0 | 1.4 | 2 |
| | TFIRE | 3.5 | 1.7 | 4 |
| | TTOT | 10.6 | 3.2 | 5 |
| | THAND | 4.2 | 2.1 | 4 |
| | IDCOR | Ø.29 | Ø.49 | 7 |
| | FIRED | Ø.71 | 0.49 | 7 5 |
| CH3 | EFFECT IDCOR | Ø.20 Ø.14 | | 5 7 |
| CHS | FIRED | Ø.14 Ø.86 | | 7 |
| | EFFECT | Ø.67 | | 6 |
| | FRAT | Ø.57 | 0.52 | 7 |
| MI28 | IDCOR | Ø.71 | 0.49 | |
| 7120 | FIRED | Ø.71 | 0.49 | 7 |
| | EFFECT | 0.80 | 0.45 | 5 |
| | ATTRIT | Ø.57 | | 7 |
| | ORD | Ø.57 | Ø.53 | |
| UHl | IDCOR | Ø.71 | 0.49 | 7 |
| J., 1 | FIRED | 0.29 | 0.49 | 7 |
| | EFFECT | 0.00 | 0.00 | 2 |
| | FRAT | 0.00 | 0.00 | 7 7 7 2 7 |
| | | ~ | ~.00 | • |

| SCENARI | O 17 DESCR | IPTIVE | S | | SCENARIO | O 18 DESCR | IPTIVES | ı |
|----------|------------|--------|---------------|-----------------------|----------|------------|---------|------|
| TARGET | VARIABLE | MEAN | SD | N | TARGET | VARIABLE | MEAN | SD |
| 1(CH3 | TDET | 1.3 | Ø.5 | 7 | 1(A7) | RDET | 11.1 | 2.2 |
| or | TIFF | 2.3 | 2.4 | 7 | • | RIFF | 7.5 | 3.7 |
| MI28 | TID | 4.0 | 1.8 | | | RID | 5.0 | 3.7 |
| or | TACQ | 4.4 | 1.3 | 7 5 5 5 5 | | TID | 21.2 | 11.1 |
| UHl) | TLOCK | 2.2 | 1.6 | 5 | | RACQ | 5.5 | 1.3 |
| | TFIRE | 1.8 | Ø.8 | 5 | | RLOCK | 4.4 | 0.0 |
| | TTOT | 8.4 | 1.8 | 5 | | RFIRE | 3.6 | Ø.1 |
| | THAND | 4.6 | 2.3 | 5 | | TTOT | 29.0 | 15.6 |
| | IDCOR | Ø.81 | Ø.49 | 7 | | IDCOR | Ø.83 | 0.41 |
| | FIRED | Ø.71 | 0.49 | 7 | | FIRED | Ø.33 | 0.52 |
| | EFFECT | | 0.00 | 5 | | EFFECT | 0.50 | Ø.71 |
| 2(CH3 | TDET | 13.1 | | 7 | | FRAT | Ø.17 | |
| or | TIFF | 2.4 | 2.9 | 7 | 2(MI24) | TDET | 9.5 | 4.9 |
| MI28 | TID | _ | 2.9 | 7 | | TIFF | 1.0 | 0.0 |
| or | TACQ | 3.2 | 2.2 | 4 | | TID | 3.0 | Ø.Ø |
| UHl) | TLOCK | - | 1.4 | 2 | | TACQ | 5.Ø | 0.0 |
| | TFIRE | | 0.0 | 3 | | TLOCK | 2.0 | 0.0 |
| | TTOT | | 1.5 | 2 3 3 3 | | TFIRE | 7.0 | |
| | THAND | 5.0 | 0.0 | 3 | | TTOT | 9.Ø | Ø.Ø |
| | IDCOR | Ø.57 | _ | 7 | | THAND | 11.0 | 7.1 |
| | FIRED | 0.43 | | 7 | | IDCOR | Ø.33 | |
| | EFFECT | = | Ø . 58 | 3 | | FIRED | Ø.33 | - |
| 3 (CH 3 | TDET | 25.3 | | 7 | | EFFECT | 0.50 | 0.71 |
| or | TIFF | 3.5 | - | 6 | | ATTRIT | Ø.17 | |
| MI28 | TID | 7.3 | • . | 7 | | ORD | 1.00 | 0.00 |
| | | | | | | | | |

Table Cl (Continued) Scenario Descriptives

SCENARIO 19 DESCRIPTIVES SCENARIO 20 DESCRIPTIVES

| OCENARI. | J 19 DESCR | 151110 | | SCENARIO 20 DESCRIPTIVES | | | | | |
|----------|-----------------|--------|--------------|--------------------------|---------|----------------|-------------|-----------------|--|
| TARGET | VARIABLE | MEAN | SD | N | TARGET | VARIABLE | MEAN | SD N | |
| l(MI? | TDET | 3.8 | 1.9 | 5 | 1(SU25) | RDET | 12.6 | 2.0 7 | |
| or | TIFF | 11.0 | 13.7 | | | RIFF | 10.5 | 2.3 6 | |
| MI28) | | 7.8 | 7.1 | 5 | | RID | 4.4 | 2.4 6 | |
| | TACQ | 8.7 | 6.7 | 4 | | TID | 27.0 | 10.3 6 | |
| | TLOCK | 4.6 | 3.1 | 5 | | RACQ | 6.4 | 2.9 6 | |
| | TFIRE | 5.7 | 6.4 | 4 | | RLOCK | 3.4 | 1.4 5 | |
| | TTOT | 16.7 | 7.7 | 4 | | RFIRE | 2.3 | Ø.7 5 | |
| | THAND | 8.0 | 9.4 | 4 | | TTOT | 34.8 | 8.0 5 | |
| | IDCOR | 0.80 | | | | IDCOR | Ø.71 | 0.49 7 | |
| | FIRED | 0.80 | | | | FIRED | Ø.71 | 0.49 7 | |
| | EFFECT | 1.00 | 0.00 | | | EFFECT | 1.00 | 0.00 5 | |
| 2(WI3 | TDE'T | 30.2 | | 6 | | ATTRIT | 0.71 | 7 | |
| or | TIFF | | 3.6 | 5 | | ORD | 0.86 | Ø.38 7 | |
| MI28) | | 5.0 | 3.9 | 6 | 2(UH6Ø | TDET | 26.0 | 11.1 7 | |
| | TACQ | 4.0 | 1.8 | 6 | or | TIFF | 8.4 | 13.8 7 | |
| | TLOCK | 8.0 | 14.5 | 5 | MI8) | | 6.0 | 2.8 6 | |
| | TFIRE | | 0.7 | 5 | | TACQ | 5.8 | 5.0 5 | |
| | TTOT | 14.2 | | 5 | | TLOCK | 3.6 | 2.7 5 | |
| | THAND | | 10.4 0.52 | | | TFIRE TTOT | 7.6 | 10.5 5 7.6 5 | |
| | IDCOR FIRED | 0.83 | | | | | 16.4 9.5 | 9.7 4 | |
| | EFFECT | Ø.75 | Ø.50 | | | THAND IDCOR | Ø.71 | Ø.49 7 | |
| 3(SU17) | | 14.6 | | 2 | | FIRED | 0.71 | Ø.49 7 | |
| 3(5017) | RIFF | 7.7 | 3.0 | 2 | | EFFECT | 0.50 | 0.58 4 | |
| | RID | 6.7 | 4.2 | 2 | UH 60 | IDCOR | 0.50 | 0.58 4 | |
| | TID | 26.5 | 9.2 | 2 | •• | FIRED | Ø.33 | Ø.52 6 | |
| | RACQ | 6.1 | 3.7 | 2 | | EFFECT | 1.00 | 0.00 2 | |
| | RLOCK | 5.3 | 3.0 | 2 | | FRAT | Ø.33 | 6 | |
| | RFIRE | 4.8 | 2.6 | 2 | MI8 | IDCOR | 0.29 | 0.49 7 | |
| | TTOT | 36.0 | 7.1 | 2 | | FIRED | Ø.43 | Ø.53 7 | |
| | IDCOR | 1.00 | 0.00 | | | EFFECT | 0.00 | 0.00 2 | |
| | FIRED | 1.00 | | | | ATTRIT | 0.00 | 7 | |
| | effect | 1.00 | 0.00 | | | ORD | 1.00 | 0.00 7 | |
| | ATTRIT | Ø.29 | | | | | | | |
| | ORD | 0.50 | 0.71 | | | | | | |
| MI? | IDCOR | 0.86 | | | | | | | |
| | FIRED | 0.86 | | | | | | | |
| | EFFECT | 0.83 | 0.41 | | | | | | |
| | ATTRIT | | | | | | | | |
| WT 20 | ORD | | 0.00 | | | | | | |
| MI28 | IDCOR | | 0.53 0.49 | | | | | | |
| | FIRED EFFECT | 1.00 | | | | | | | |
| | ATTRIT | | | | | | | | |
| | ORD | - | 0.53 | | | | | | |
| | | | | , | | | | | |

NOTE: No engagement data on target number 3